



JFE

OCTG SERVICE HANDBOOK



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1 Introduction to JFE Premium Connections

The JFE connections detailed within this running manual book have been designed and developed by JFE Steel Corporation, Japan. All JFE connections are manufactured by JFE Steel Corporation or by authorized manufacturing licensees.

JFE has been supplying steel tubulars & premium connections into the OCTG market since the 1980's and continues to develop products to overcome the increasing complexity of Oil & Gas wells.

The information detailed within this running manual is to assist the user with a successful operation. If further information or field service is required, please visit www.jfetec.com for the contact information in your region.

This running manual is for information purpose only and JFE Steel Corporation does not accept any responsibility for any loss, damage or injury resulting from the use of the information herein. The information is then requested to be undertaken solely by the customers own risk and responsibility.

All the JFE connections detailed within this report, i.e. FOX, JFEBEAR, JFETIGER, and JFELION are all registered trademarks (™).



2 Alternative JFE Connection Options

2.1 100% & 101% Tensile Efficient (TE) Coupling

For various FOX & JFEBEAR sizes, the option of a 100% & 101% tensile efficient coupling OD exists. The standard coupling OD's were based on the original connection design, however with further connection design refinement, the 100% & 101% TE options provide a slimmer coupling OD while still maintaining the full connection performance properties.

2.2 45° Standard Chamfer & 20° Optional Bevel Options

For the FOX, JFEBEAR, JFETIGER & JFELION connections, to assist with smoother running operations and reduce couplings 'hanging up', a 20 degree optional bevel option is available. If the 20 degree optional bevel is selected, it should be noted that the coupling bearing face load rating is reduced. The maximum bearing face load ratings are shown on the CDS.



2.3 Special Clearance Options

Special clearance options are available for all JFE connections (see the specific connection special clearance OD section for further info). The special clearance options provide a further, slimmer connection OD, however this then impacts the connections yield strength and therefore the overall string tensile strength. If the coupling is special clearance, a black band will be painted adjacent to the material grade colour identification bands, plus the stencil description will include SC.

Stencil Example

JFEBEAR™ SC80 L80-13Cr 7" 29#, where the coupling OD tensile efficiency is 80%.

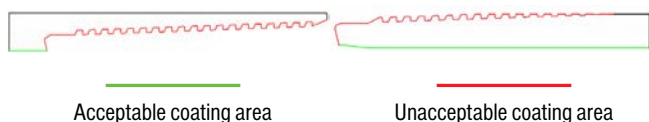


2.4 GRE Liner

Glass Reinforced (GRE) liner is available on various sizes of FOX, JFEBEAR & JFELION connections.

2.5 Internal Plastic Coating Guidelines

Internal plastic coatings can be applied to JFE premium connections, specifically FOX, JFEBEAR, JFETIGER & JFELION. If a plastic coating exists within the tubing ID, no coating shall be applied to the thread, seal, and torque shoulder areas. The figures below show the acceptable areas for plastic coating applications on JFE premium connections.



2.6 Non-standard Products

The JFELION and JFEBEAR connections offer a number of non-standard products for various customer projects around the globe. These products will be identified as non-standard by the stencilling on the connection, e.g. JFEBEAR HT, and JFELION CBR, to list a few. For datasheets and more information with respect to these connections, please contact your local JFE-TC office.

2.7 Maximum Torque with Sealability

The Maximum Torque with Sealability (MTS) value is available for JFEBEAR and JFELION connections only. This torque value is the maximum figure the connection can be assembled to while maintaining sealability.

The torque can be applied during tong make-up on the rig floor, or alternatively, during rotation downhole. If applying on the rig floor, it is recommended that all mill end couplings are torqued to the MTS value during production at the steel mill or manufacturing licensee.

For smaller diameter connections, MTS is not available due to the low margin between the current maximum torque and structural yield torque.

All MTS values can be found on the specific connection data sheets available at www.jfetc.com.

2.8 Fatigue Life Performance

Connection fatigue information is typically required for drilling with casing or riser applications.

Various full scale fatigue testing has been performed on the connection product line offered by JFE Steel Corporation.

For more information on specific connection fatigue life, please contact your local JFE-TC office.

2.9 JFE Clear-Run Product Guide

JFE Clear-Run is an environmentally friendly running system which is available on JFEBEAR, JFETIGER and JFELION. Clear Glide is the primary component of the Clear-Run system which offers excellent long-term corrosion and galling resistance, therefore allowing products to arrive at the rig site in a ready to run condition. Clear Glide has a yellow OSPAR rating.

End finishing of pin and box connections for the JFE Clear Run system is critical where Clear-Plate (a proprietary electroplating technology) must be applied to chrome alloy boxes to ensure successful make-ups.

See the specific connection end finish requirement section for further info for the JFE Clear Run end finish requirements.

The following table describes where Clear-Glide can be purchased and Clear-Plate can be applied.

Clear-Glide Stockists	Licensed Clear-Plate Facilities
GB Premium Services (USA) Beattie (Canada) MITE (Europe)	MP Eastern Limited (UK) S&S Plating (USA) Guerrero Plating Technology (USA) Sobena Offshore Sdn Bhd KSB (Malaysia) Isiziz Plating Co. Ltd (Japan) Iwase Plating Co. Ltd (Japan)

3 Pipe Storage & Handling

3.1 General Storage in Yard

It is recommended that upon receipt of tubular goods, remove from the export packing and store in an indoor, dry atmosphere if possible. 13Cr tubulars should be inspected immediately after arrival to ensure no water contamination exists which can cause corrosion during storage. The following points should be adhered to for the storage of tubular goods:

- 1 Grades 13Cr or above are generally kept in wrap type systems
- 2 Store pipes at least 18 inches above ground level to prevent contamination
- 3 Rest pipe on supports, adequately spaced to prevent bending of the pipe
- 4 Hardwood strips/dunnage to be present between layers of pipe so no weight is applied to couplings
- 5 It is recommended for chromium tubulars, especially 13Cr, that hardwood strips/dunnage be lined with plastic or rubber to avoid direct contact with the tubulars. This will prevent potential pitting
- 6 Bumper rings can also be utilised to avoid metal contact
- 7 Pipe should not be stacked higher than 10ft
- 8 Pipe & connections should be inspected periodically, i.e. every 1 to 3 months
- 9 During inspection the protectors are likely to be removed, therefore once inspection is completed ensure storage compound provides 100% coverage of connection prior to reinstallation of protector

3.2 General Storage at Rig Site

Before transferring the pipe to the pipe deck, it is recommended to inspect the area and ensure the correct materials i.e. dunnage is available before the operation begins. The following points are also recommended for storage at the rig site for all steel grades:

- 1 Hardwood should be placed on top of the deck beams before the first lot of pipe is laid down
- 2 Between each pipe layer, at least two rows of hard wooden spacers should exist, perpendicular to pipe length to avoid bending during storage, pipe OD contact, and ease of inspection
- 3 Keep protectors fitted during storage to avoid damage to the connections
- 4 Storage compound should be applied to the connection to avoid corrosion if pipe is not rig prepped

3.3 High Chrome/CRA Handling Guidelines

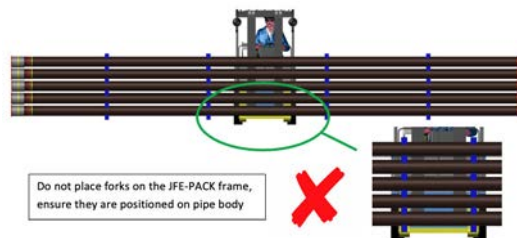
- 1 Handle joints individually using nylon slings (recommended). Do not use metal wire rope
- 2 Avoid rough handling i.e. colliding joints together, as this can result in localised work hardening
- 3 In the case of threading, padded pipe tables, padded forks and non-steel drifts should be utilised
- 4 If storing for long periods, indoor storage is recommended
- 5 Low stress/non marking dies should be utilised for tongs, slips & elevators when running high chrome tubulars

3.4 Storage & Handling of Tubulars in JFE-PACK

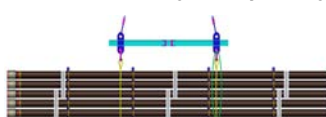
The following steps are recommended when handling pipe contained within the JFE-PACK system:

- Lift the JFE-PACK system by crane or forklift as shown in the following images

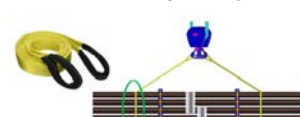
Correct Forklift Handling Practice



Crane with beam hanger and nylon slings



Crane with nylon slings

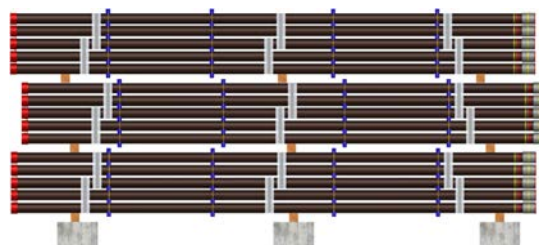


- Ensure slings are positioned on the pipe body, not the packaging
- Ensure JFE-PACK is lifted vertically to eliminate any possible damage due to impact

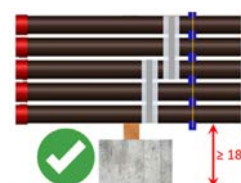
The following steps are recommended storing pipe contained within the JFE-PACK system:

- When stacking JFE-PACKS, place hardwood strips/dunnage with minimum size 105mm x 105mm x required length between each pack to ensure packs do not get damaged
- Maximum height should be no more than 10ft (2.1m) high, a maximum of 4 packs
- Storage racks should be high enough to avoid contact with the ground and have sufficient runners to prevent pipe from sagging (min. 3 runners for R3)
- Rack pipes at least 18" (457 mm) above ground. If the area where pipe is being stored is prone to flooding, then the height from ground should be increased accordingly. JFE do not recommend laying the JFE-PACK or pipe directly on the ground.

JFE-PACK with appropriate support and hardwood/dunnage



JFE-PACK stored at correct height above ground



3.5 JFE-PACK Assembly Procedure

This section details the equipment, tooling and assembly instructions for the JFE-PACK which is used to transport pipe from the JFE Steel mill to the customer's yard and/or rig site.

The JFE-PACK is a proprietary composite type packaging system offered by JFE Steel to avoid metal to metal pipe contact during transportation and storage.

For further information regarding the packing technology, please contact info@jfetc.com

All the preparation, packing and handling steps detailed within this document are to ensure optimum performance of the JFE-PACK. JFE Steel Corporation does not accept any responsibility for any loss, damage or injury resulting from the use of the information herein. The information is then requested to be undertaken solely by the customers own risk and responsibility.

3.5.1 Tooling and Equipment Required

Tooling	Equipment
• Torque wrench • Metal/steel banding tool	• Metal banding • Polypropylene sheet • JFE-PACK nut • JFE-PACK T-bolt/rod • Appropriate JFE-PACK spacer • JFE-PACK frame (bottom, middle and upper sections)

3.5.2 Packing Preparation

Prior to pipe packing, the bottom section of the JFE-PACK frame should be positioned appropriately so the pipe weight is supported equally.

The bottom section of the JFE-PACK is easily identifiable – it is the only section that has a 'hook type' fixture on each end. The hook should face down as shown in the image below.

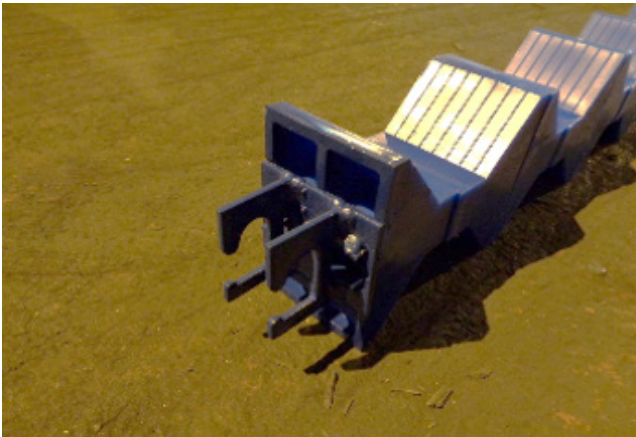


Image 1 – Bottom section of JFE-PACK with 'hook' – positioned downwards

3.5.2-1 JFE-PACK Bottom Section Positioning Criteria (R2)

For pipe lengths 25 to 34ft, the bottom section should be positioned as shown in figure 1. The pipes to be packed should be measured to acquire the overall length, and the centre determined. Once the centre is determined, the left and right hand side bottom sections can be positioned.

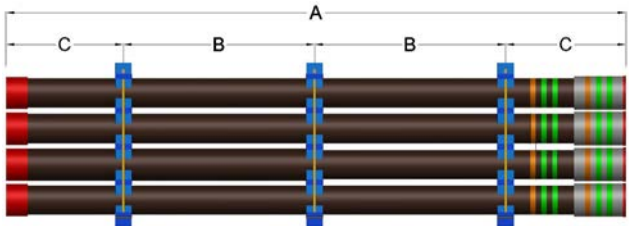


Figure 1 – JFE-PACK Positioning (Only applicable for R2 lengths)

Table 1 – Example of JFE-PACK Positioning lengths for R2 lengths

A	B	C
25ft	Max 10ft	Min 2.5ft
34ft	Max 11.25ft	Min 5.75ft

3.5.2-2 JFE-PACK Bottom Section Positioning Criteria (R3)

Pipe lengths 34.1 to 48ft, the bottom section should be positioned as shown in figure 2. The pipes to be packed should be measured to acquire the overall length, and the centre determined. Once the centre is determined, the left and right hand side bottom sections can be positioned.

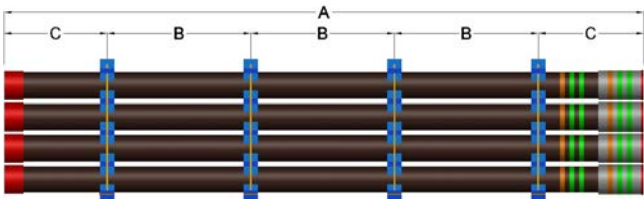


Figure 2 – JFE-PACK Positioning (Only applicable for R3 lengths)

Table 2 – Example of JFE-PACK Positioning lengths for R3 lengths

A	B	C
34.1ft	Max 9.5ft	Min 2.8ft
48ft	Max 11.25ft	Min 7.125ft

Lengths for B & C are adjustable, however adequate area should exist in order to assemble the polypropylene and metal banding as explained in section 5.2.

3.5.3 JFE-PACK Bottom Section Positioning Criteria (Pup Joints)

If pup joints are packed using the JFE-PACK system, only two frames shall be required. This is applicable to lengths from 2 to 10ft. The JFE-PACK sections shall be positioned at equal distances along the length of the pup joint. See the figure below for more information.

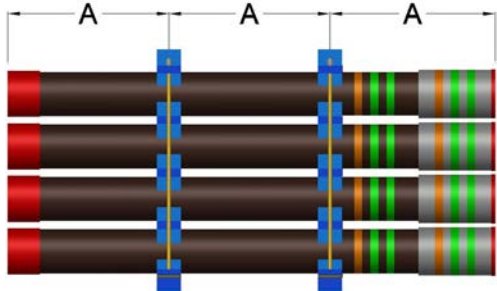


Figure 3 – JFE-PACK Positioning (Applicable for various pup joint lengths)

Table 3 – JFE-PACK Positioning lengths for pup joint lengths, 2 to 10ft

A
Equal lengths (min: 0.67ft / max: 3.33ft)

3.5.4 Packing and Stacking

- 1 Once the bottom sections of the JFE-PACK have been positioned accordingly on level ground, the pipes can be lowered onto the frame section.
- 2 Ensure that the mill ends are aligned before positioning the middle section of the JFE-PACK directly above the bottom frame section. The middle section of the JFE-PACK is shown below.

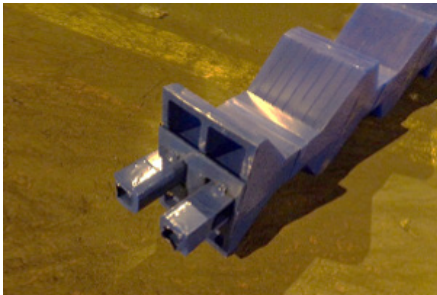


Image 2 – Middle section of JFE-PACK with two straight arms

Once the middle sections have been positioned, the next column of pipe can be lowered carefully onto the middle frame section.

- 3 Steps 2 and 3 can be repeated until the maximum number of columns has been achieved. The maximum numbers of columns are shown in table 4 on page 14.
- 4 Finally, once the stacking has been complete, the final top section should be placed directly above the uppermost middle section. The top section of the JFE-PACK is shown below.

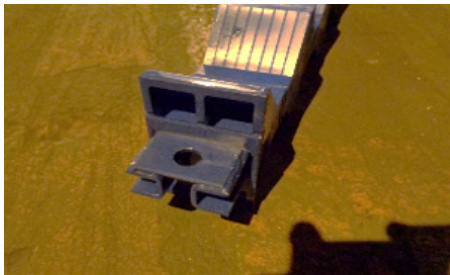


Image 3 – Top section of JFE-PACK with flat plate and hole – facing upwards

Important note: If insufficient pipes remain to completely fill the uppermost column of the JFE-PACK, the pipes shall be positioned using figures 4 & 5 as examples - do not stack to one side.

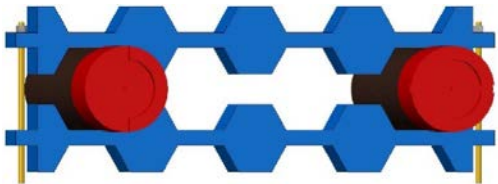


Figure 4 – two pipes remain for upper column

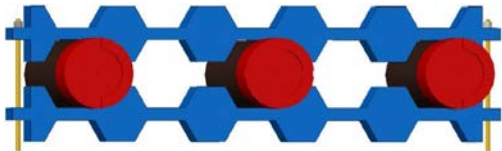


Figure 5 – three pipes remain for upper column

Table 4 – Maximum pipes per row (width) and column (height)

Outer Diameter (inch)	Nominal weight (lb./ft.)	Max pieces per row	Max pieces per column	Maximum pieces per JFE-PACK	
				R2	R3
				3 frames	4 frames
2 3/8	4.6	9	8	72	63
2 3/8	5.1	9	7	63	54
2 3/8	5.8	9	6	54	45
2 3/8	6.2	9	6	54	45
2 7/8	6.4	7	7	49	42
2 7/8	7.7	7	6	42	35
2 7/8	8.6	7	5	35	28
3 1/2	9.2	6	6	36	30
3 1/2	10.2	6	5	30	24
3 1/2	12.7	6	4	24	18
4	13.0	5	5	25	20
4	14.8	5	5	25	20
4	16.5	5	4	20	15
4 1/2	11.6	5	5	25	25
4 1/2	12.6	5	5	25	20
4 1/2	13.5	5	5	25	20
4 1/2	15.1	5	4	20	15
5	15.0	4	4	16	16
5	18.0	4	4	16	16
5 1/2	15.5	4	4	16	16
5 1/2	17.0	4	4	16	16
5 1/2	20.0	4	4	16	12
5 1/2	23.0	4	4	16	12
6	18.8	3	3	9	9
6 5/8	23.3	3	3	9	9
6 5/8	28.0	3	3	9	9
6 5/8	32.0	3	3	9	9
7	26.0	3	3	9	9
7	29.0	3	3	9	9
7	32.0	3	3	9	9
7	38.0	3	3	9	6
9 5/8	43.5	2	2	4	4
9 5/8	53.5	2	2	4	4

3.5.5 Securing the JFE-PACK

Insert bolts and secure

- 1 Once the frames are in the correct positions, following the instructions set out in section 4, the T-section bolt and nut (see image 4 below) should be assembled to secure the frames in place. See table 5 for required bolt lengths.
- 2 The T-section of the bolt should be positioned within the downward facing hook of the bottom JFE-PACK section and the threaded end passed through the hole of the upper JFE-PACK section.
- 3 The M16 lock nut should then be screwed onto the bolt and tightened using the torque wrench to a maximum torque of 177ft-lb. (240Nm). If this torque is exceeded, it may deform the JFE-PACK – see image below showing the T-section bolt and nut in torqued state.



Image 4 – T-section bolt and nut

Table 5 – Bolt length table for tubing and casing (inches)

OD (inch)	OD (mm)	Number of layers							
		1	2	3	4	5	6	7	8
2 3⁄8	60.3	4.33	7.87	11.81	15.75	19.69	23.62	27.17	30.71
2 7⁄8	73.0	4.92	9.25	13.19	17.52	21.85	26.38	30.71	-
3 1⁄2	88.9	5.71	10.43	15.75	20.28	25.20	30.31	-	-
4	101.6	6.30	11.81	16.93	21.85	27.56	-	-	-
4 1⁄2	114.3	6.69	12.20	18.31	24.21	30.31	-	-	-
5	127.0	7.87	13.98	19.69	26.38	-	-	-	-
5 1⁄2	139.7	7.87	14.57	21.26	28.54	-	-	-	-
6	152.4	7.87	15.75	22.83	-	-	-	-	-
6 3⁄8	168.3	9.06	16.93	25.20	-	-	-	-	-
7	177.8	9.25	17.72	25.98	-	-	-	-	-
7 3⁄8	193.7	9.84	18.90	-	-	-	-	-	-
8	203.2	10.63	19.69	-	-	-	-	-	-
8 1⁄2	215.9	10.63	20.28	-	-	-	-	-	-
8 3⁄4	219.1	11.81	22.83	-	-	-	-	-	-
9 3⁄8	244.5	11.81	22.83	-	-	-	-	-	-

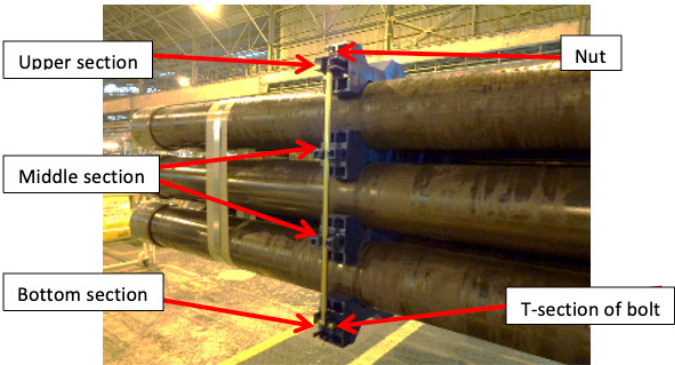


Image 5 – JFE-PACK with T-section bolt and nut in secure position

Steel Banding with Polypropylene Sheet

The final part of the packing process, to provide extra stiffness and secureness, is the assembly of polypropylene sheet and steel banding over the OD of the pipes.

A few important factors shall be followed when banding the pipe together:

- 1 The polypropylene sheet length should be at least 4 inch (102mm) longer than the length required to wrap around the pipe – see image 6 below
- 2 The polypropylene sheet width shall be a minimum of 4.5 inch (114mm) on either side of the metal band
- 3 Edge of the polypropylene sheet shall be 8" +/- 0.5" (203mm +/- 13mm) from edge of the JFE-PACK frame
- 4 Metal band width shall be minimum 1.25" (32mm)
- 5 The distance between metal bands positioned side by side shall be within 12" (305mm)

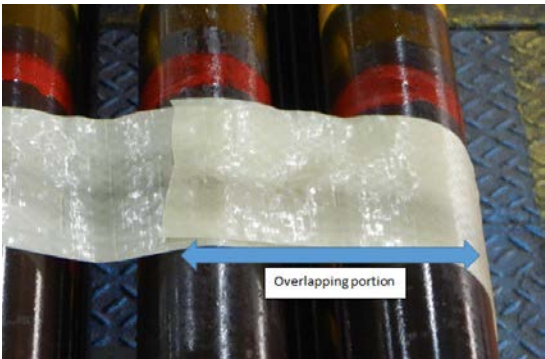


Image 6 – polypropylene overlapping technique



Image 7 – polypropylene overlapping technique

Steel Banding Positioning Guidelines

Depending on the length of pipe, i.e. R2 or R3 and pipe outer diameter, the number of bandings required shall change. See figures 6 to 9 for more details.

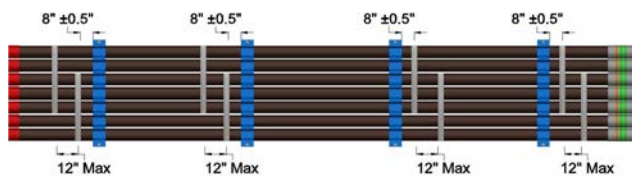


Figure 6 – Applicable to R3 joints where OD is $\leq 2 \frac{7}{8}$ " (Birdseye view)

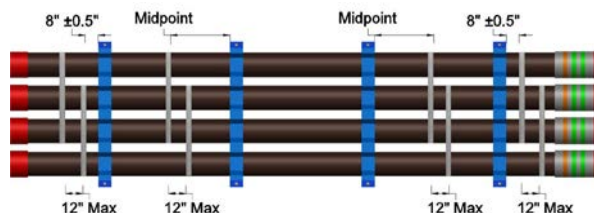


Figure 7 – Applicable to R3 joints where OD is $> 2 \frac{7}{8}$ " (Birdseye view)

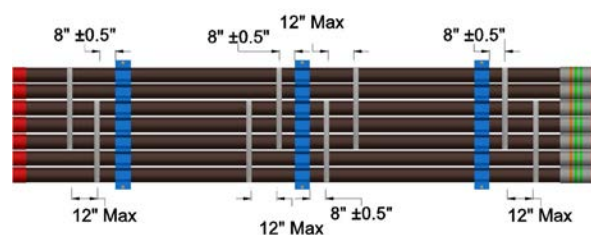


Figure 8 – Applicable to R2 joints where OD is $\leq 2 \frac{7}{8}$ " (Birdseye view)

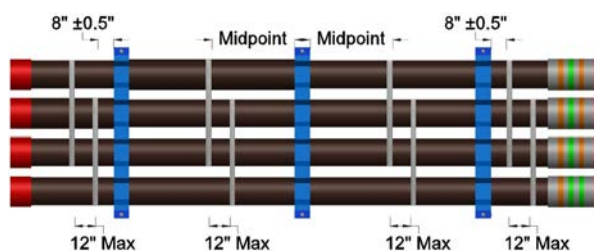


Figure 9 – Applicable to R2 joints where OD is $> 2 \frac{7}{8}$ " (Birdseye view)

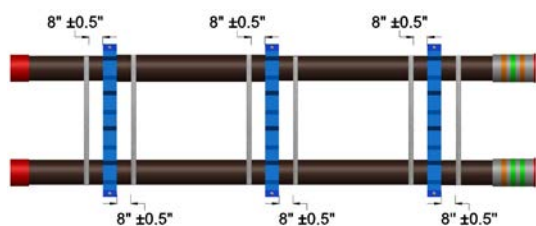


Figure 10 –

Applicable to R2 joints where the uppermost column of the JFE-PACK is not full
Birdseye view of top column only

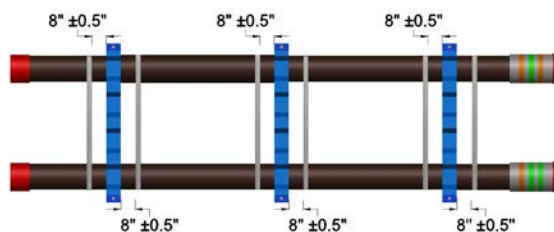


Figure 11 –

Applicable to R3 joints where the uppermost column of the JFE-PACK is not full
Birdseye view of top column only

3.5.6 Safety Guidance for Unpacking or JFE-PACK

- 1 Do not stand directly in front of the metal band when cutting loose. Due to the tension in the metal band, it may spring suddenly which could cause injury if the person is hit by it.
- 2 Do not attempt to pull the remaining metal band from between the pipes once cut in order to avoid injury. Wait until pipes have been lifted by appropriate method and metal bands which have fallen to the floor can then be collected.
- 3 When loosening the bolts from the JFE-PACK, perform in stages, i.e. loosen slightly on one side, followed by loosening slightly on opposite side. By performing this in stages, the person will allow for the frame to relax equally.

3.5.7 Safety Guidance for Unpacking or JFE-PACK

The following points should be adhered to when handling loaded JFE-PACK's to avoid pipe or JFE-PACK frame damage:

- 1 Handle one JFE-PACK at a time
- 2 Use a spreader bar if lifting using a crane to distribute weight appropriately and ensure nylon slings are positioned around the pipe body, not the JFE-PACK
- 3 If using a forklift, ensure the forks are lined with nylon or wood and position the forks so contact is made to the pipe body only, not the JFE-PACK
- 4 When stacking JFE-PACK's, position at least two hardwood strips/dunnage (min size: 4" x 4") on the top of each JFE-PACK to avoid damage
- 5 It is recommended for chromium ($\geq 13\%Cr$) tubulars, that hardwood strips/dunnage be lined with plastic or rubber to avoid direct contact with the tubulars. This will help to lessen the potential of pitting. See JFE's handling and storage guidelines for additional information
- 6 No more than 4 to 6 (depending on pipe size) JFE-PACK's should be stacked on top of each other at any one time to avoid exceeding a height of 10ft
- 7 If loading pipe onto a heavy goods vehicle, position hardwood strips/dunnage on the bed of the vehicle at suitable positions to avoid JFE-PACK contact with HGV bed. Ensure hardwood strips do not contact with the JFE-PACK

4 Approved thread compounds

This procedure recommends the thread compounds that can be used to make-up JFE connections.

JFE do not recommend the use of thread compounds containing PTFE (Teflon®) for premium connections.

List of Approved Thread Compounds include, but are not limited to:

Connection	Material Grade	API Modified [1]	Weatherford Lube Seal	Jet-Lube HPHT
FOX®	Carbon	✓	✓	✗
	9Cr to 17Cr	✓	✓	✗
	CRA	✓	✓	✗
JFEBEAR®	Carbon	✓	✓	✗
	9Cr to 17Cr	✓	✓	✗
	CRA	✓	✓	✗
JFETIGER®	Carbon	✓	✓	✗
	9Cr to 17Cr	✓	✓	✗
	CRA	✓	✓	✗
JFELION®	Carbon	✓	✓	✗
	9Cr to 17Cr	✓	✓	[8]
	CRA	✓	✓	[4]
JFERABBIT®	Carbon	✓	✗	✗

Connection	Material Grade	BOL 4010NM	TOPCO Green Seal II	Clear-Glide™ [2]	BOL 2000
FOX®	Carbon	✓	✗	✓	✗
	9Cr to 17Cr	≤5.5" [7]	✗	✓	✗
	CRA	≤5.5" [7]	✗	✓	✗
JFEBEAR®	Carbon	✓	✗	✓	✗
	9Cr to 17Cr	≤5.5" [7]	✗	✓	✗
	CRA	≤5.5" [7]	✗	✓	✗
JFETIGER®	Carbon	✓	✗	[4]	✗
	9Cr to 17Cr	[6]	✗	[4]	✗
	CRA	[6]	✗	[4]	✗
JFELION®	Carbon	≤5.5" [5][6]	[3]	[4]	✗
	9Cr to 17Cr	≤5.5" [7]	✗	[4]	✗
	CRA	≤5.5" [7]	✗	[4]	✗
JFERABBIT®	Carbon	✗	✗	✗	✓

[1] Thread compounds that are in compliance with API RP 5A3 Annex A can be used on JFE connections. Different names are given and are dependent on the thread compound manufacturer.

[2] Clear-Glide™ is to be used only with Clear-Run™ prepared tubulars, i.e. when the proper end finishing is applied.

[3] For use in geothermal well applications.

[4] Contact your local JFETC office for further information.

[5] Can be applied to sizes larger than 5.5" with as machined pins if Clear-Plate™ is applied to the coupling/box.

[6] Can be applied to sizes larger than 5.5" with Mn phosphate on the couplings, if the pin ends are abrasive blasted in accordance with JFE specifications.

[7] Can be applied to sizes larger than 5.5" if Clear-Plate™ is applied to the coupling/box.

[8] Can be applied to sizes ≤ 5.5" if Clear-Plate™ is applied to the coupling/box.

JFE continues to evaluate the use of thread compounds. It is recommended to contact your nearest JFE-TC office for further information if other compounds that are not listed are required. Please continuously refer to www.jfetec.com for the most updated list and technical data.

This table is for informational purpose only.

4.1 Application of thread compound

A thin, even coat of approved thread compound should be applied to the pin and box so the entire seal and thread areas are fully covered and the profiles are discernible.

Before application, ensure the connections are thoroughly cleaned and dried and the thread compound has been stirred to obtain a homogenous consistency.

Application of the thread compound should be performed with a non-metallic soft bristle moustache brush as shown in Fig 6.1 or similar.

The pictures below show a few examples of poor and good doping practises.

✗ Too little thread compound applied



✗ Excessive thread compound applied



✗ Too little thread compound applied



✗ Excessive thread compound applied



✓ Correct amount of thread compound applied



✓ Correct amount of thread compound applied



4.2 Application of Clear-Glide (Clear-Run)

A thin, even coat of Clear Glide should be applied to the pin and box thread and seal areas to achieve a semi-transparent appearance where the profiles are discernible and inspection through the Clear Glide is possible.

Before application, ensure the connections are thoroughly cleaned and dried.

Application of the Clear Glide should be performed with a non-metallic moustache brush as shown in figure 6.1 or similar.

The pictures below show a few examples of poor and good Clear Glide applications.

✗ Too little thread compound applied



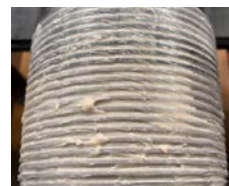
✗ Excessive thread compound applied



✗ Too little thread compound applied



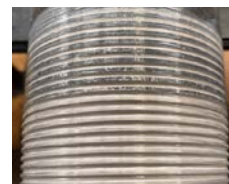
✗ Excessive thread compound applied



✓ Correct amount of thread compound applied



✓ Correct amount of thread compound applied



5.1 Horizontal Connection Make-up

A number of accessories will usually be assembled onshore in workshops prior to shipment to the rig site. The information detailed within this section is intended to assist the onshore make-up operations to ensure a smooth and successful operation. This is applicable to all JFE premium connections.

5.1.1 Equipment required

- Uncontaminated thread compound that has been thoroughly stirred prior to application (see section 4 or the relevant connection section for the list of approved thread compounds)
- Uncontaminated non-metallic, soft bristle brush or moustache brush as shown in figure 6.1 for compound application
- Appropriate sized horizontal power tong with suitable load cell, i.e. a 50kft-lb power tong is usually unsuitable for a make-up torque of 2,000ft-lb. The torque turn monitoring system should have the ability to record 1,000 data points per turn
- Ensure the horizontal power tong Tailstock/back-up and headstock/ tong have the appropriate sizes dies to ensure an even gripping pressure around the circumference of the pin and box accessories
- The horizontal power tong should have sufficient torque capacity in the event a break-out is required. Typically, break-out is 20% greater than the make-up torque
- Obtain the correct mill end make-up torque from the relevant technical specification (JFE-TP-J-101) or www.jfetc.com
- The mill end optimum make-up torque is the average of the field optimum torque and maximum torque

5.1.2 Certification

Ensure the horizontal power tong is within calibration. Calibration intervals should be no greater than 6 months.

Power Tong Calibration Interval	
Assembly shops/JFE licensees: ≤ 12 months	Tubular running service company (offshore/onshore): ≤ 6 months

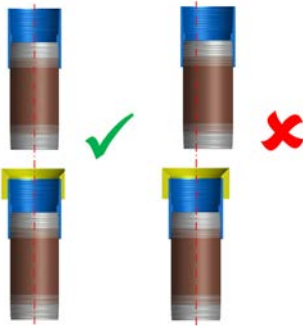
5.1.3 Procedure

- Ensure the pin and box connections are cleaned and dried thoroughly, followed by a visual inspection
- Check section 13.9 & 12.8 to determine whether Molybdenum Disulphide should be applied to the pin and box seal and shoulder areas. If yes, apply uniformly and ensure it dries before dope application
- Next, apply a thin even coat of the approved thread compound (see section 4.1 & 4.2) to both pin and box
- Screw on coupling/accessory to the pin or vice versa and tighten to the hand tight position. A strap wrench or chain tong can be used to assist with this operation
- Position the horizontal tailstock and headstock around the assembly and grip in appropriate areas. Note: An anti-deformation plug is recommended for the box field end if gripping over this area. Note 2: Recommend to use spirit level to ensure proper alignment is achieved.
- Make-up the connection using the appropriate torque figures (www.jfetc.com and section 10.7 / 11.7 / 12.7 / 13.7). Do not exceed 6RPM during the make-up
- Check the graph meets the acceptance criteria (detailed in the specific connection make-up acceptance criteria section)
- Finally, clean excess compound from ID and end drift as per API 5CT or customer requirements
- Apply a suitable or specific storage compound before applying the thread protector

5.2 Recommended Checks

Before running JFE connections, the following preliminary checks should be carried out:

- Ensure the rig alignment is correct as per the image below:



- Ensure the correct thread dope compound (see section 4 or the relevant connection section for the list of approved thread compounds for approved compounds) & sufficient amount exists to complete the entire job. Do not use if expiry date has passed and JFE recommends that a new pail of dope is used for each running job
- If pipe measuring is required on pipe deck, remove protectors and measure from pin face to box face. This is the total length and the effective length can be achieved using the following calculation:

Effective length = total length – make-up loss

(Make-up loss can be found on the connection data sheet)

- Check the equipment and surrounding areas are safe and free from any potential hazards
- Check the correct elevators and stabbing guides are compatible with the coupling and pipe diameters – slip type elevators should be used for special bevel and special clearance couplings
- Check the tong and torque turn equipment are calibrated and hold a valid calibration certificate
- Check the load cell is suitable for the upcoming running job, i.e. a 50kft-lb power tong is unsuitable for a make-up torque of 2,000ft-lb
- Ensure the torque turn equipment is computer controlled. Recommended resolution = 1000 DP/Turn
- Ensure the correct make-up torque values for the JFE connection are applied
- Check the tong dies, slips and slip type elevators are appropriate for the running job i.e. low stress/non-marking for high chrome/CRA/Sour Service material¹. See section 6.4
- If drifting, precautions should be taken to ensure the nose/seal areas are not damaged. A Teflon or Nylon drift is recommended. If possible, install open ended thread protectors when carrying out this operation. Drift sizes are specified in section 5.3.
- If running chromium steel connections, nylon slings and strap wrenches should be available
- Ensure a sufficient quantity of spare thread protectors are available in the event the pipe is pulled
- Locate and inspect all required pipe and accessories to be installed and ensure the correct connection and material grade exists
- When cleaning the connections prior to running, remove the storage compound using high pressure hot water, cleaning solvent, i.e. soap, then ensure connections are completely dry. Do not use diesel or kerosene as this may leave a thin film on the threads and affect the friction during make-up
- Re-install clean thread protectors before lifting operations up to the vee door begin

The torque figures for all JFE connections can be found at www.jfetc.com.

All the major tong operators' offer dies for use with their tong equipment when running corrosion resistant alloy (CRA) tubulars. It is important when running CRA tubulars to minimise or prevent surface penetration as this can lead to stress raisers and assist with stress corrosion cracking (SCC) and/or sulphide stress cracking (SSC).

5.3 Drifting

- It is recommended to perform the drift operation from box to pin end to avoid dragging dirt and debris from the ID of the pipe into rig prepared box connections
- The drift may also be known as a 'rabbit' where the length is shorter than the required length as per API 5CT. The use of this is at the customers discretion.
- A Teflon or Nylon drift is recommended for all operations, however when drifting chromium or CRA steel grades a Teflon or Nylon drift mandrel must be used
- The drift mandrel should meet the API specifications (5CT E.28) as shown in the following table:

Standard drift sizes:

Size (inch)	Standard Length (inch)	Drift Diameter (inch)
Tubing		
≤ 2 7/8	42	d-(3/32)
> 2 7/8 to 8 5/8	42	d-(1/8)
> 8 5/8 to 10 3/4	42	d-(5/32)
Casing		
< 9 5/8	6	d-(1/8)
9 5/8 to 13 3/8	12	d-(5/32)
> 13 3/8	12	d-(3/16)

d = nominal pipe internal diameter

Alternative/special drift sizes:

Size (inch)	Weight (lb/ft)	Standard Length (inch)	Drift Diameter (inch)
7	23.00	6	6.250
7	29.00	6	6.125
7	32.00	6	6.000
7 3/4	46.10	6	6.500
8 5/8	32.00	6	7.875
8 5/8	40.00	6	7.625
9 5/8	40.00	12	8.750
9 5/8	53.50	12	8.500
9 5/8	58.40	12	8.375
9 5/8	66.90	12	8.500
10 3/4	45.50	12	9.875
10 3/4	55.50	12	9.625
11 3/4	42.00	12	11.000
11 3/4	60.00	12	10.625
11 3/4	65.00	12	10.625
13 3/8	72.00	12	12.250
14	114.00	12	12.250
14	115.00	12	12.250

6 Running Information

6.1 Guidelines

- During the pick-up operation where the pipe will travel up the vee door, the single joint elevator should fit neatly around the pipe behind the coupling
 - If drifting from the top of vee door, precautions should be taken to ensure the nose/seal areas are not damaged. A Teflon or Nylon drift is recommended. If possible, install open ended thread protectors when carrying out this operation
 - Inspect the box connection at this stage and ensure no damage exists
 - To avoid a potential drop hazard downhole, it is recommended to apply the approved thread compound to the dry, clean box at this stage – excess dope compound should be removed. Application of the thread compound should be performed with a non-metallic soft bristle moustache brush as shown in Fig 6.1 or similar
 - Throughout travel up the vee door, the pin protector should remain tightly assembled to prevent damage
 - Alternatively, if pick-up and laydown equipment is used, these should be lined with plastic/rubber when handling chromium, CRA & sour service grades. Wood should not be used to line the bucket as wooden splinters can cause problems during make-up and running
 - Do not remove the pin thread protector until the joint is hanging vertically in the derrick area – this will help to prevent damage from mishandling. Do not remove directly above the open coupling secured in the rotary table/slips to avoid contamination
 - If 'quick type' protectors are utilised, the shipping protector should be removed immediately prior to lifting up the vee door and the quick type protector installed before travel – the 'quick type' protector should fit correctly and cover the entire connection
 - Once the pin protector is removed, inspect to ensure no damage exists before applying the approved thread compound over the dry, clean connection – excess dope compound should be removed. Application of the thread compound should be performed with a non-metallic soft bristle moustache brush as shown in Fig 6.1 or similar
 - In some cases, the connections may arrive at the rig in a 'ready to run' state, therefore no dope application will be required on the drill floor
 - Install a clean, correctly sized stabbing guide to the coupling and securely fasten
 - Once the pin is directly above the box immediately before the stabbing process, check the alignment once again
 - The initial one or two turns during the stabbing process are critical to achieve correct thread engagement. For small diameters, a strap wrench or chain tong can be used to assist with this process, and for large diameters the tong in low speed can be utilised
 - For chrome and CRA material, it is recommended to use a strap wrench to walk the connection in. This will reduce the chance of cross-threading and possible galling damage
 - If the connection becomes locked during stabbing, rotate the pipe in the reverse direction until the connection drops, also known as 'bumps'
 - Once the stabbing operation is completed, the final make-up operation can commence
 - Position power tongs around the connection and ensure the tong grips pipe to pipe at the appropriate gripping pressure. See section 6.4 for jaw/die permissible depth mark information
 - During the final make-up stage, the maximum rotational speed should not exceed 6 RPM
 - If a tubing connection ($\leq 4 \frac{1}{2}$ ") has three failed make-up attempts, lay down and select a new pin
 - If a casing connection (≥ 5 ") has two failed make-up attempts, lay down and select a new pin
- It is recommended to clean make-up dies, slip dies and elevator dies every 50 joints to avoid slippage and subsequent damage to the pipe/coupling body.
- It is recommended to use slip type elevators for special clearance OD and 20° optional bevel couplings.



Fig 6.1 - Moustache Brush - Recommended application brush for thread compound

JFE Clear-Run Running Guide

- JFE Clear Run prepared pipe will likely be delivered to the rig site in a ready to run condition, therefore no cleaning is required. Clear Glide acts as a long-term storage and running compound
- A visual inspection can be performed through the Clear-Glide due the semi-transparent appearance
- Ensure contamination does not occur which may result in running issues, e.g., yielding
- Check www.jfetc.com for the latest torque figures as Clear Run make-up torques are different from the standard product

6.2 Running Dual Completions

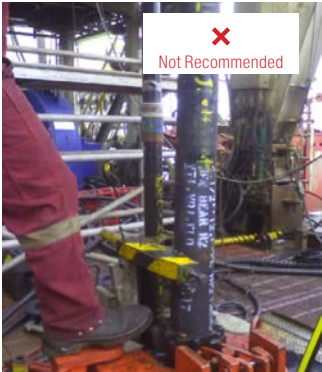
When running dual completions, it is recommended to use a dual completion tong as shown below:



Using a dual completion tong eliminates the requirement for a spreader bar

A spreader bar will cause side loading on the connection as shown in the image to the right. This is not recommended.

For additional running information, follow the steps as detailed in running guidelines (Section 6.1)



Photos courtesy of Frank's International

6.3 Running Pipe in Stands

- Stands should be racked with pin protectors fitted & seated on a wooden board/non-metallic surface
- Ensure a weight compensator is being used when running stands. It is recommended the compensator be set at 50 to 100lbs more than the total stand weight.
- Once the connection has been stabbed correctly, rotate the pipe anti-clockwise to ensure correct thread engagement has been achieved. The tong can then be used to run in the casing to the hand tight position, not exceeding 6RPM
- For small diameter casing, care should be taken to prevent the stand from bowing during stabbing and make-up operations
- Follow the steps as detailed in the above running guidelines (Section 6.1)
- When racking back stands post break-out, protectors should be assembled tightly on the pin connections. There should also be a sufficiently sized hole within the protector to allow for drainage of rain water and fluids from the ID
- If a box protector is installed, a sufficient hole should exist to prevent pressure build up when lowering the stand
- Stands should be placed on wood or rubber mats during storage
- If stands are to be stored for prolonged periods, the pin and box connection should be cleaned and storage compound applied before assembly of the protector

For additional information, please refer to the full running manual (JFE-TP-M-001) which can be found at www.jfetec.com.

6.4 Jaw/Die Depth Mark Information

6.4.1 Low Alloy Criteria

OD Size (inch)	Coupling OD Max Grip Mark (inch) as per API 5CT E.36	Pipe OD Max Grip Mark as per API 5CT SR2 Requirement (JFE-TC Recommendation)
< 3 1/2	0.025	5% of Nominal Wall Thickness
3 1/2 to 6.068	0.030	
> 6 5/8	0.040	

6.4.2 High Chrome and CRA Criteria

For material with chrome content from 9%Cr to 17%Cr, JFE recommend the use of low stress or non-marking jaws/dies.

For CRA materials, i.e. API 5CRA groups 2 to 4, non-marking jaws/dies are recommended however it is up to discretion of the end user.

For high chrome and CRA material, it is recommended that a maximum tong depth of 0.015" or 5% of nominal wall thickness (whichever is less), exists on both the pipe and coupling surface.

Note: To promote good industry practise, it is recommended to treat sour service grade steels in a similar fashion to CRA in order to avoid stress raisers in high concentration hydrogen (H2S) environments.

6.5 Orientating Well Features

JFE Steel offer an option where connections can be manufactured to assist with the alignment of well features to specific orientations, whether onshore or offshore. This feature is typically required for gauge mandrels, dual completions, etc.

It is strongly recommended that a trained JFE representative be present for any orientation process.

For more information, please contact your local JFE-TC office.

7 Break-out & Re-running Information

7.1 Break-out

In order to break-out the connection, the tong should be positioned so that the back-up jaws grip over the mill end coupling OD. Do not apply excessive jaw gripping pressure.



Photo courtesy of Weatherford International

- Ensure the back-up grips on the tong are the correct size for the coupling OD
- Apply tension to the joint or stand; the applied load should equal approx. the weight of the joint or stand. It is recommended to utilise a weight compensator
- Apply the break-out torque slowly and maintain a steady speed to avoid damage
- Never use a hammer or other hard object to assist with the break-out as this may cause damage
- The torque required to break-out the connection may be considerably more compared to make-up
- For chrome connections, once the torque is low enough, it is recommended to use a strap wrench to walk the connection out
- To avoid damage, ensure a stabbing guide of the correct size is assembled over the coupling before lifting the joint out of the corresponding box
- For whatever reason the connection is being broken out for, if not being immediately re-run, clean the connection before applying storage compound or Clear Glide and fitting the appropriate thread protector. Clear Glide in an approved storage compound for JFE connections.

7.2 Re-running

Prior to re-running, it is recommended that the connections are inspected by a qualified JFE field service representative to ensure they are acceptable to run in hole again.

- If a tubing connection ($\leq 4 \frac{1}{2}$ ") has three failed make-up attempts, lay down and select a new pin
- If a casing connection (≥ 5 ") has two failed make-up attempts, lay down and select a new pin

8 Thread Locking Procedure

This guideline outlines the method for applying thread locking compound and the make-up acceptance criteria.

8.1 Locking Compound Information

The locking compound manufacturer’s instructions should be followed to ensure the compound is used correctly. The locking compound should be mixed and applied at the last moment prior to make-up to prevent make-up issues, e.g., high shoulder torque. The compound begins to cure immediately once the catalyst is introduced causing the friction factor to increase over time.

8.2 Application Procedure

- 1 The thread locking compound should be applied to the pin thread run-out area as shown below in figure 8.2.1. Under no circumstances should the locking compound be applied to the seal and torque shoulder areas. Thread compound can be applied to the pin nose and torque shoulder areas.

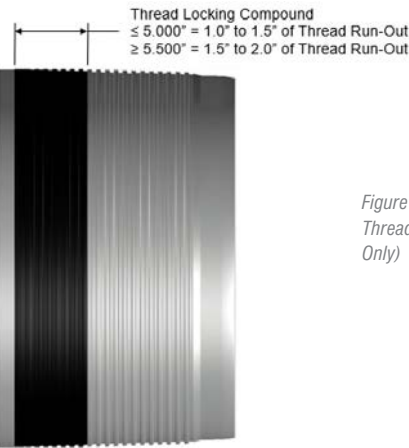


Figure 8.2.1 – Thread Lock Application (Pin Only)

- 2 Apply a thin, even coat of the approved thread compound to cover the thread, seal and torque shoulder area shown in figure 8.2.2 below. The compound should cover approximately 50% of the box connection where seal and thread forms should be discernible after application.

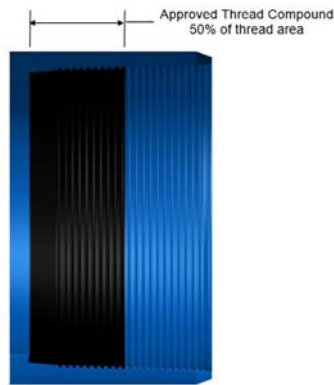


Figure 8.2.2 – Thread Compound Application (Box Only)

- 3 When making up the connection, standard torque values with a friction factor of 1.0 shall be used.

8.3 Torque Values

Depending on the type of locking compound and connection size, increasing the torque range may be required. The maximum torque with sealability (MTS) value can be used as a maximum torque value. When using the MTS, adjust the optimum torque to 95% of the MTS while maintaining the original minimum torque value. If an MTS value is not shown on the connection data sheet, please contact your local JFETC office for further assistance.

Torque setting example:

Torque	MTS	MTS value on CDS
	Optimum (Dump)	95% of MTS value
	Minimum	Minimum

Thread lock make-up graph examples are shown in figures below.

Figure 8.3.1 – Example where optimum torque has been set at 95% of the MTS value

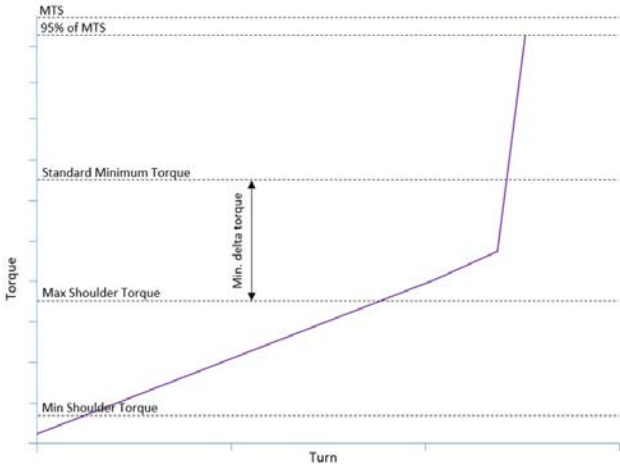
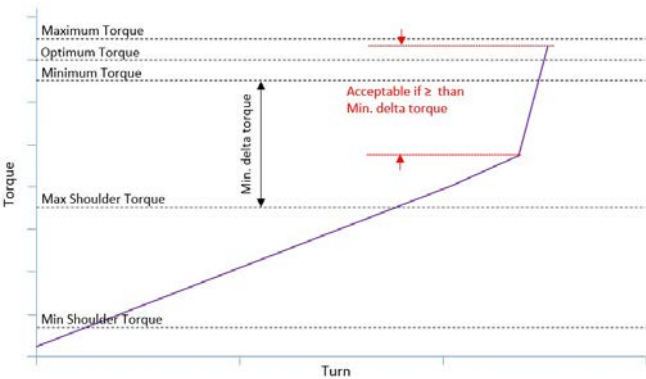


Figure 8.3.2 – The minimum delta torque is achieved after shouldering during make-up, the make-up is acceptable



9 Pipe and Coupling Colour Code Information

9.1 API 5CT

Pipe Grade	Coupling	Pipe Body	Pipe Grade	Coupling	Pipe Body
J55 Tubing			P110		
J55 Casing			P110-1Cr		
K55			P110-RY		
N80 Type 1			P110-CY		
N80 Type Q			P110-E		
L80 Type 1			P110-HC		
L80 Type 13Cr			P110-HCX		
L80-1Cr			P110-MS		
L80-HC			C110		
L80-HCX			C110-HC		

Pipe Grade	Coupling	Pipe Body	Pipe Grade	Coupling	Pipe Body
C90 Type 1			C110-HCX		
R95			C110-XS		
R95-HC			C110-XSHC		
R95-HCX			C110-XSXHC		
T95 Type 1			Q125		
T95-HC			Q125-RY		
T95-HCX			Q125-CY		
T95-E			Q125-HC		
T95-EHC			Q125-HCX		
T95-EHCX					

9.2 JFE Chrome

Pipe Grade	Coupling	Pipe Body	Pipe Grade	Coupling	Pipe Body
JFE-13Cr-80			JFE-HP2-13Cr-110		
JFE-13Cr-85			JFE-HP2-13Cr-95M		
JFE-13Cr-95			JFE-UHP-15Cr-125		
JFE-HP1-13Cr-95			JFE-UHP-15Cr-135		
JFE-HP1-13Cr-110			JFE-UHP-17Cr-110		
JFE-HP2-13Cr-95			JFE-UHP-17Cr-125		
JFE-HP2-13Cr-110M					

9.3 JFE Carbon

Pipe Grade	Coupling	Pipe Body	Pipe Grade	Coupling	Pipe Body
JFE-80T			JFE-95SS		
JFE-80S, 85S, 80TS			JFE-95L		
JFE-85SS			JFE-110T		
JFE-80L			JFE-110S		
JFE-90S			JFE-110SS		
JFE-90SS			JFE-110L		
JFE-95T			JFE-125T		
JFE-95S, 95TS			JFE-125S		
JFE-125L			JFE-140T		
JFE-125V			JFE-140V		
JFE-125M					

9.4 API 5CRA

Pipe Grade	Coupling	Pipe Body	Pipe Grade	Coupling	Pipe Body
22Cr-110			Alloy C726-110		
22Cr-125			Alloy C726-125		
25Cr-80			Alloy G3-110		
25Cr-110			Alloy G3-125		
25Cr-125					
28Cr-110					
28Cr-125					



10.1 Design Features

Figure 10.1.1 – Alloy Box Detail



Figure 10.1.2 – Carbon Box Detail



Figure 10.1.3 – Alloy & Carbon Pin Detail



OD (inch)	Threads per Inch (TPI)
2 3/8 to 2 7/8	8
3 1/2 to 4	6
4 1/2 to 13 3/8	5

10.2 Interchangeability

FOX connections with differing weights are interchangeable within a given OD. Rules when mixing differing weights & grades:

- The lower make-up torque of the lighter weight/ lower grade connection should be used
- If pin weight is heavier, a step will extrude into pipe bore from pin
- If box weight is heavier, a step will extrude into pipe bore from box
- Couplings with differing weights may have differing OD's

The following tables provide examples of the rules when mixing various weights and grades for FOX.

Figure 10.2.1 – Differing Weights + Identical Grades (ID step = 0.031", Applied torque is the lesser torque value of the combined connections.)

3 1/2" JFEBEAR	Weight	Grade	Nominal Connection ID	Minimum Field Torque	Optimum Field Torque	Maximum Field Torque
	lb/ft	ksi	inch	ft-lb		
Box	10.2	80	2.915	4040	4490	4940
Pin	12.7	80	2.853	4710	5230	5760
Applicable Torque						
Step/side (inch)		0.031		4040	4490	4940

Figure 10.2.2 – Identical Weights + Differing Grades (No ID step, Applied torque is the lesser torque value of the combined connections.)

3 1/2" JFEBEAR	Weight	Grade	Nominal Connection ID	Minimum Field Torque	Optimum Field Torque	Maximum Field Torque
	lb/ft	ksi	inch	ft-lb		
Box	10.2	80	2.915	4040	4490	4940
Pin	10.2	95	2.915	4690	5210	5730
Applicable Torque						
Step/side (inch)		0		4040	4490	4940

Figure 10.2.3 – Differing Weights + Differing Grades (ID step = 0.042", Applied torque is the lesser torque value of the combined connections.)

4 1/2" JFEBEAR	Weight	Grade	Nominal Connection ID	Minimum Field Torque	Optimum Field Torque	Maximum Field Torque
	lb/ft	ksi	inch	ft-lb		
Box	15.2	95	3.852	7110	7900	8690
Pin	12.6	80	3.936	4860	5400	5940
Applicable Torque						
Step/side (inch)		0.042		4860	5400	5940

10.3 Field Inspection

Field Inspection Tools

The following tools are commonly used but not limited to during field inspection & repair procedures:

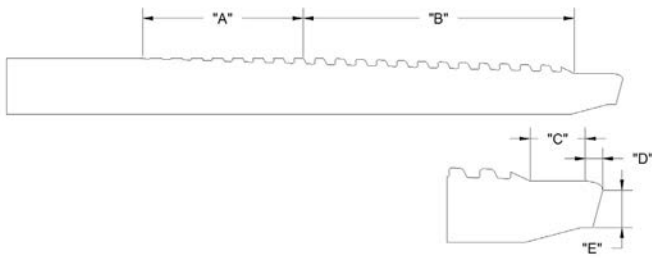
- Depth Gauge
- Fine Tooth Triangle File
- Scotch Brite
- Emery Cloth
- Soft Stone
- Vernier Calipers
- Rotary Tools¹

¹ Rotary tools can only be used by qualified JFE field service personnel.

A selection of field repair tools are shown in the image below.



10.3.1 FOX Pin Visual Inspection Criteria & Guidelines



Condition: Corrosion

Zone	Criteria	Action
A, B, C, E	All surfaces. Pitting less than 0.004" (0.1mm) deep or minor surface corrosion	Hand repair with soft bristle (no steel wire) brush or emery cloth
	Deeper than 0.004" (0.1mm)	Cut off & re-thread
D	No pitting acceptable	If present, cut off & re-thread
	Light surface corrosion (rust)	Hand repair with scotch brite or #400 emery cloth. Do not alter seal dimension. Repair should be made in a larger area than actual surface corrosion and should move around the circumference of the seal

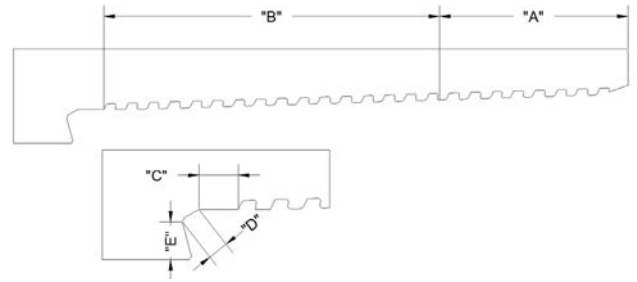
Condition: Burr, Tear, Ding, Mash, Scratch

Zone	Criteria	Action
A, B, C, E	All surfaces. Any condition which could cause galling, i.e. conditions described greater than 0.010" (0.3mm)	Hand repair with a fine triangle file; emery cloth or rotary tool ¹ . Repair should be made in a larger area than actual effected area and should move around the helix of the thread. Otherwise - reject.
D	Not acceptable	If present, cut off & re-thread

Condition: Bead peening on carbon steel (≤ 4 1/2") and high chrome steel

Zone	Criteria	Action
A, B, C, D, E	Inspect for peened surface. If previously made-up, normal wear is expected and is acceptable	Bead peen if not present

10.3.2 FOX Box Visual Inspection Criteria & Guidelines



Condition: Corrosion

Zone	Criteria	Action
A, B, C, E	Slight imperfections and light surface corrosion, i.e. Less than 0.004" (0.1mm)	Hand repair with soft bristle (no steel wire) brush, emery cloth or scotch brite
	All other imperfections deeper than 0.004" (0.1mm)	Reject or re-thread
D	No pitting acceptable	Reject or re-thread
	Light surface corrosion (rust)	Hand repair with scotch brite or #400 emery cloth. Do not alter seal dimension. Repair should be made in a larger area than actual surface corrosion and should move around the circumference of the seal
Coupling OD, ID Bore & Bearing Face	Pitting or corrosion less than 0.020" (0.5mm) deep	Grind to the bottom of the pit & smooth edges. Keep within product tolerances.
	Deeper than 0.020" (0.5mm)	Reject or re-thread

Condition: Burr, Tear, Ding, Mash, Scratch

Zone	Criteria	Action
A, B, C, E	All surfaces. Any condition which could cause galling, i.e. conditions described greater than 0.010" (0.3mm)	Hand repair with a fine triangle file or emery cloth. Repair should be made in a larger area than actual effected area and should move around the helix of the thread. Otherwise - reject.
D	Not acceptable	If present, cut off & re-thread

Condition: Manganese phosphate

Zone	Criteria	Action
A, B, C, D, E	Must be present. Inspect for medium grey surface colour. If previously made-up, normal wear is expected and is acceptable	Manganese phosphate if not present, reject, or re phosphate

Condition: Copper-plate and Clear-Plate™

Zone	Criteria	Action
A, B, C, D, E	Inspect the electroplated surface. Oxidation or discolouration of the plated surface is acceptable. If previously made-up, normal wear is expected and acceptable. Any delamination of plating is cause for reject	If holiday/ delamination exists, reject or re-plate

10.4 Approved Thread Compounds

This procedure recommends the thread compounds that can be used to make-up JFE connections.

JFE do not recommend the use of thread compounds containing PTFE (Teflon®) for premium connections.

List of Approved Thread Compounds include, but are not limited to:

FOX Approved Thread Compounds

Connection	Material Grade	API Modified [1]	Weatherford Lube Seal	Jet-Lube HPHT
FOX®	Carbon	✓	✓	✗
	9Cr to 17Cr	✓	✓	✗
	CRA	✓	✓	✗

Connection	Material Grade	BOL 4010NM	TOPCO Green Seal II	Clear-Glide™ [2]	BOL 2000
FOX®	Carbon	✓	✗	✓	✗
	9Cr to 17Cr	≤5.5" [3]	✗	✓	✗
	CRA	≤5.5" [3]	✗	✓	✗

[1] Thread compounds that are in compliance with API RP 5A3 Annex A can be used on JFE connections. Different names are given and are dependent on the thread compound manufacturer.

[2] Clear-Glide™ is to be used only with Clear-Run™ prepared tubulars, i.e. when the proper end finishing is applied.

[3] Can be applied to sizes larger than 5.5" if Clear-Plate™ is applied to the coupling/box.

JFE continues to evaluate the use of thread compounds. It is recommended to contact your nearest JFE-TC office for further information if other compounds that are not listed are required. Please continuously refer to www.jfetc.com for the most updated list and technical data.

This table is for informational purpose only.

10.5 Lifting Plugs

Figure 10.5.1 – Example of main body for lift plug (seal removed)



The following points shall be adhered to for FOX lift plugs:

- The lift plug shall be manufactured from low alloy steel with a specified minimum yield stress (SMYS) of 110ksi, and a maximum yield stress of 140ksi.
- The lift plug shall be bead peened, phosphated or copper-plated as per the relevant procedures. Once machining has been completed, weld on handles can be installed to assist with handling and assembling operations. If handles are installed, they shall be of appropriate size and orientated 0° and 180°.
- The lift plug is low torque and therefore a power tong is not required. Final positioning before lifting operation can be achieved using the handles or strap wrench/chain tong

The following information shall be low stress stamped on the lift plug where drifting operations are not required:

Size, All weights, grade and FOX Lift Plug
Licensee code plus manufacturing date
For lifting a maximum of three joints only

Stencil Example

9 5/8" All weights AISI 4145 110ksi FOX Lift Plug
SI-081; 22nd April 2021
For lifting a maximum of three joints only

The following information shall be low stress stamped on the lift plug where drifting through the plug is required:

Size, weight, grade and FOX
Bore ID = XXXX
Licensee code plus manufacturing date
For lifting a maximum of three joints only

Example

2 7/8" 6.4# AISI 110ksi FOX Lift Plug
Bore ID = 2.441"
SI-081; 22nd April 2021
For lifting a maximum of three joints only

10.6 Make-Up Acceptance Criteria

Figure 10.6.1 – Example of an acceptable, typical FOX make up graph

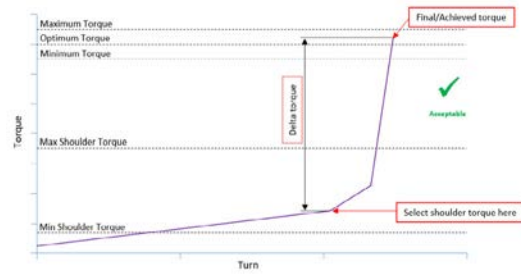


Figure 10.6.2 – Example of an acceptable FOX make-up graph (Shoulder point is below maximum shoulder)

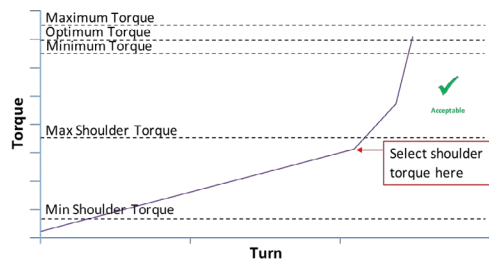


Figure 10.6.3 – Example of an acceptable FOX make up graph (Minor slippage during thread engagement)

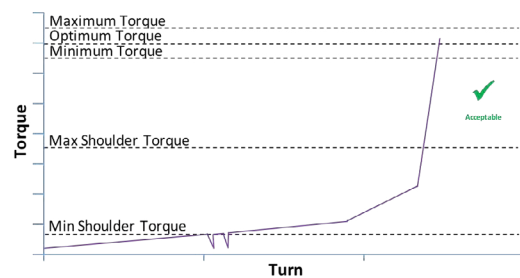
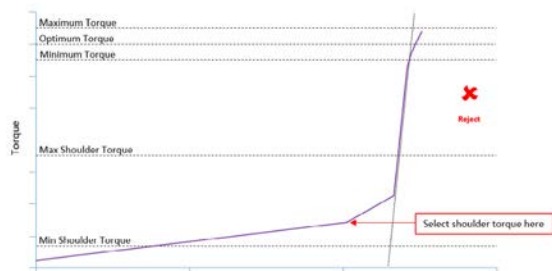


Figure 10.6.4 – Example of an unacceptable FOX make-up graph (loss of linearity is not acceptable). *If in doubt, please contact your local JFE Technical Center*



Possible causes of the unacceptable graph profile but not limited to, are as follows:

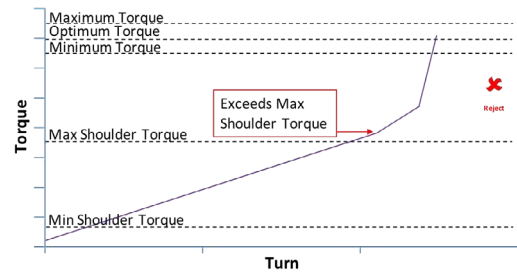
- Shoulder torque has not been selected correctly
- Dope is contaminated
- Pin or box dimensions are out with the tolerance range
- The surface treatment for the pin or box is out with the tolerance range
- Friction factor of dope is too low
- Load cell error

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists

It should be noted that if the delta turns are greater than 0.1, however no loss of linearity exists, the graph can be accepted.

Figure 10.6.5 – Example of an unacceptable FOX make up graph (Exceeds Max Shoulder Torque)



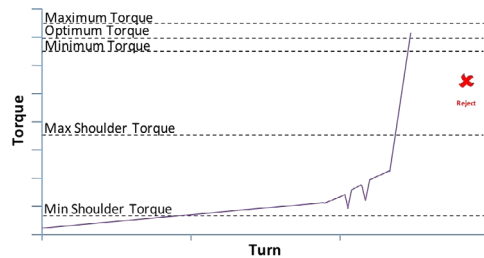
Possible causes of the unacceptable graph profile but not limited to, are as follows:

- Friction factor of dope is too high
- Dope is contaminated
- Pipe may not be straight
- Pin or box dimensions are out with the tolerance range
- The surface treatment for the pin or box is out with the tolerance range

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists

Figure 10.6.6 – Example of an unacceptable FOX make up graph (Slipping during seal engagement)



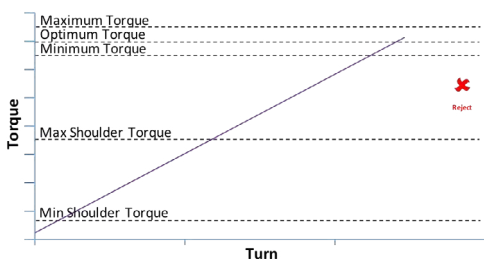
Possible causes of the unacceptable graph profile but not limited to, are as follows:

- Pipe may not be straight
- Jaw of power tong is worn out or dirty

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists

Figure 10.6.7 – Example of an unacceptable FOX make up graph (No clear shoulder torque)



Possible causes of the unacceptable graph profile but not limited to, are as follows:

- Friction factor of dope is too high
- Dope is contaminated
- Pipe may not be straight
- Pin or box dimensions are out with the tolerance range
- The surface treatment for the pin or box is out with the tolerance range

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists



11.1 Design Features

Figure 11.1.1 – Box Detail



Figure 11.1.2 – Pin Detail



OD (inch)	Threads per Inch (TPI)
2 3/8 to 2 7/8	8
3 1/2 to 4	6
4 1/2 to 9 5/8	5

11.2 Interchangeability

JFEBEAR connections with differing weights are interchangeable within a given OD. Rules when mixing differing weights & grades:

- The lower make-up torque of the lighter weight/ lower grade connection should be used
- If pin weight is heavier, a step will extrude into pipe bore from pin
- If box weight is heavier, a step will extrude into pipe bore from box
- Couplings with differing weights may have differing OD's
- JFEBEAR & JFEBEAR HT are interchangeable

The following tables provide examples of the rules when mixing various weights and grades for JFEBEAR.

Figure 11.2.1 – Differing Weights + Identical Grades (ID step = 0.031", Applied torque is the lesser torque value of the combined connections.)

3 1/2" JFEBEAR	Weight	Grade	Nominal Connection ID	Minimum Field Torque	Optimum Field Torque	Maximum Field Torque
	lb/ft	ksi	inch	ft-lb		
Box	10.2	80	2.915	4040	4490	4940
Pin	12.7	80	2.853	4710	5230	5760
Applicable Torque						
Step/side (inch)		0.031		4040	4490	4940

Figure 11.2.2 – Identical Weights + Differing Grades (No ID step, Applied torque is the lesser torque value of the combined connections.)

3 1/2" JFEBEAR	Weight	Grade	Nominal Connection ID	Minimum Field Torque	Optimum Field Torque	Maximum Field Torque
	lb/ft	ksi	inch	ft-lb		
Box	10.2	80	2.915	4040	4490	4940
Pin	10.2	95	2.915	4690	5210	5730
Applicable Torque						
Step/side (inch)		0		4040	4490	4940

Figure 11.2.3 – Differing Weights + Differing Grades (ID step = 0.042", Applied torque is the lesser torque value of the combined connections.)

4 1/2" JFEBEAR	Weight	Grade	Nominal Connection ID	Minimum Field Torque	Optimum Field Torque	Maximum Field Torque
	lb/ft	ksi	inch	ft-lb		
Box	15.2	95	3.852	7110	7900	8690
Pin	12.6	80	3.936	4860	5400	5940
Applicable Torque						
Step/side (inch)		0.042		4860	5400	5940

11.3 Field Inspection

Field Inspection Tools

The following tools are commonly used but not limited to during field inspection & repair procedures:

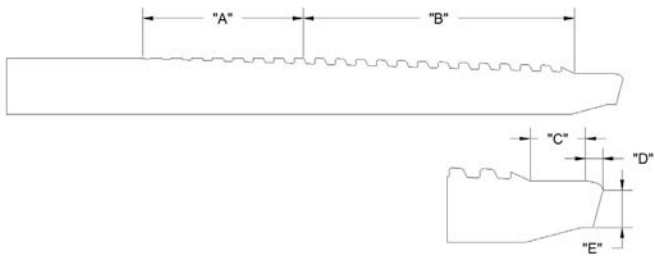
- Depth Gauge
- Fine Tooth Triangle File
- Scotch Brite
- Emery Cloth
- Soft Stone
- Vernier Calipers
- Rotary Tools¹

¹ Rotary tools can only be used by qualified JFE field service personnel.

A selection of field repair tools are shown in the image below.



11.3.1 JFEBEAR Pin Visual Inspection Criteria & Guidelines



Condition: Corrosion

Zone	Criteria	Action
A, B, C, E	All surfaces. Pitting less than 0.004" (0.1mm) deep or minor surface corrosion	Hand repair with soft bristle (no steel wire) brush or emery cloth
	Deeper than 0.004" (0.1mm)	Cut off & re-thread
D	No pitting acceptable	If present, cut off & re-thread
	Light surface corrosion (rust)	Hand repair with scotch brite or #400 emery cloth. Do not alter seal dimension. Repair should be made in a larger area than actual surface corrosion and should move around the circumference of the seal

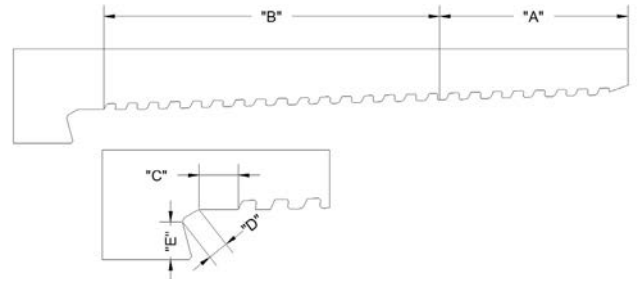
Condition: Burr, Tear, Ding, Mash, Scratch

Zone	Criteria	Action
A, B, C, E	All surfaces. Any condition which could cause galling, i.e. conditions described greater than 0.010" (0.3mm)	Hand repair with a fine triangle file; emery cloth or rotary tool ¹ . Repair should be made in a larger area than actual effected area and should move around the helix of the thread. Otherwise - reject.
D	Not acceptable	If present, cut off & re-thread

Condition: Bead peening on carbon steel (≤ 4 1/2") and high chrome steel

Zone	Criteria	Action
A, B, C, D, E	Inspect for peened surface. If previously made-up, normal wear is expected and is acceptable	Bead peen if not present

11.3.2 JFEBEAR Box Visual Inspection Criteria & Guidelines



Condition: Corrosion

Zone	Criteria	Action
A, B, C, E	Slight imperfections and light surface corrosion, i.e. Less than 0.004" (0.1mm)	Hand repair with soft bristle (no steel wire) brush, emery cloth or scotch brite
	All other imperfections deeper than 0.004" (0.1mm)	Reject or re-thread
D	No pitting acceptable	Reject or re-thread
	Light surface corrosion (rust)	Hand repair with scotch brite or #400 emery cloth. Do not alter seal dimension. Repair should be made in a larger area than actual surface corrosion and should move around the circumference of the seal
Coupling OD, ID Bore & Bearing Face	Pitting or corrosion less than 0.020" (0.5mm) deep	Grind to the bottom of the pit & smooth edges. Keep within product tolerances.
	Deeper than 0.020" (0.5mm)	Reject or re-thread

Condition: Burr, Tear, Ding, Mash, Scratch

Zone	Criteria	Action
A, B, C, E	All surfaces. Any condition which could cause galling, ie. conditions described greater than 0.010" (0.3mm)	Hand repair with a fine triangle file or emery cloth. Repair should be made in a larger area than actual effected area and should move around the helix of the thread. Otherwise - reject.
D	Not acceptable	If present, cut off & re-thread

Condition: Manganese phosphate

Zone	Criteria	Action
A, B, C, D, E	Must be present. Inspect for medium grey surface colour. If previously made-up, normal wear is expected and is acceptable	Manganese phosphate if not present, reject, or re phosphate

Condition: Copper-plate and Clear-Plate™

Zone	Criteria	Action
A, B, C, D, E	Inspect the electroplated surface. Oxidation or discolouration of the plated surface is acceptable. If previously made-up, normal wear is expected and acceptable. Any delamination of plating is cause for reject	If holiday/ delamination exists, reject or re-plate

11.4 Approved Thread Compounds

This procedure recommends the thread compounds that can be used to make-up JFE connections.

JFE do not recommend the use of thread compounds containing PTFE (Teflon®) for premium connections.

List of Approved Thread Compounds include, but are not limited to:

JFEBEAR Approved Thread Compounds

Connection	Material Grade	API Modified [1]	Weatherford Lube Seal	Jet-Lube HPHT
JFEBEAR®	Carbon	✓	✓	✗
	9Cr to 17Cr	✓	✓	✗
	CRA	✓	✓	✗

Connection	Material Grade	BOL 4010NM	TOPCO Green Seal II	Clear-Glide™ [2]	BOL 2000
JFEBEAR®	Carbon	✓	✗	✓	✗
	9Cr to 17Cr	≤5.5" [3]	✗	✓	✗
	CRA	≤5.5" [3]	✗	✓	✗

[1] Thread compounds that are in compliance with API RP 5A3 Annex A can be used on JFE connections. Different names are given and are dependent on the thread compound manufacturer.

[2] Clear-Glide™ is to be used only with Clear-Run™ prepared tubulars, i.e. when the proper end finishing is applied.

[3] Can be applied to sizes larger than 5.5" if Clear-Plate™ is applied to the coupling/box.

JFE continues to evaluate the use of thread compounds. It is recommended to contact your nearest JFE-TC office for further information if other compounds that are not listed are required. Please continuously refer to www.jfetc.com for the most updated list and technical data.

This table is for informational purpose only.

11.5 Lifting Plugs

Figure 11.5.1 – Example of main body for lift plug (seal removed)



The following points shall be adhered to for JFEBEAR lift plugs:

- The lift plug shall be manufactured from low alloy steel with a specified minimum yield stress (SMYS) of 110ksi, and a maximum yield stress of 140ksi.
- The lift plug shall be bead peened, phosphated or copper-plated as per the relevant procedures. Once machining has been completed, weld on handles can be installed to assist with handling and assembling operations. If handles are installed, they shall be of appropriate size and orientated 0° and 180°.
- The lift plug is low torque and therefore a power tong is not required. Final positioning before lifting operation can be achieved using the handles or strap wrench/chain tong

The following information shall be low stress stamped on the lift plug where drifting operations are not required:

Size, All weights, grade and JFEBEAR Lift Plug
Licensee code plus manufacturing date
For lifting a maximum of three joints only

Stencil Example

9 5/8" All weights AISI 4145 110ksi JFEBEAR Lift Plug
SI-081; 22nd April 2021
For lifting a maximum of three joints only

The following information shall be low stress stamped on the lift plug where drifting through the plug is required:

Size, weight, grade and JFEBEAR Lift Plug
Bore ID = XXXX
Licensee code plus manufacturing date
For lifting a maximum of three joints only

Example

4.5" 12.6# AISI 110ksi JFEBEAR Lift Plug
Bore ID = 3.958"
SI-081; 22nd April 2021
For lifting a maximum of three joints only

11.6 Make-Up Acceptance Criteria

Figure 11.6.1 – Example of an acceptable, typical JFEBEAR make up graph

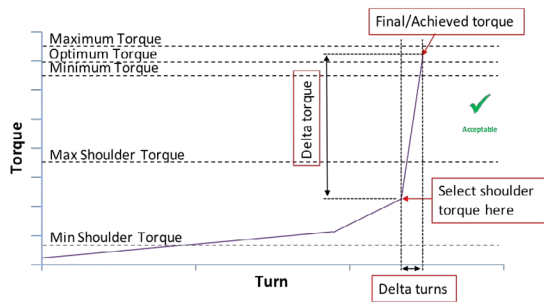


Figure 11.6.2 – Example of an acceptable JFEBEAR make-up graph (minor loss of linearity within 0.1 delta turns). If delta turns are higher than 0.1, however the graph remains linear, the graph is acceptable.

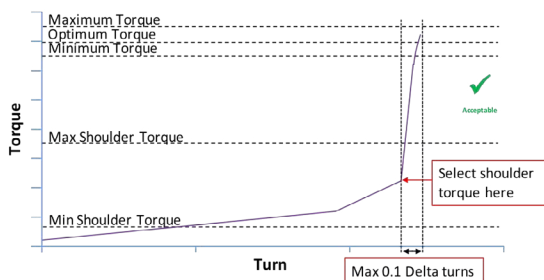


Figure 11.6.3 – Example of an acceptable JFEBEAR make up graph (Minor slippage during thread engagement)

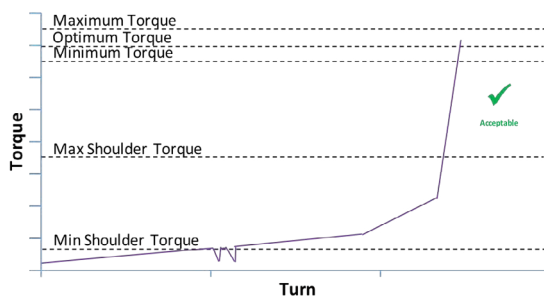
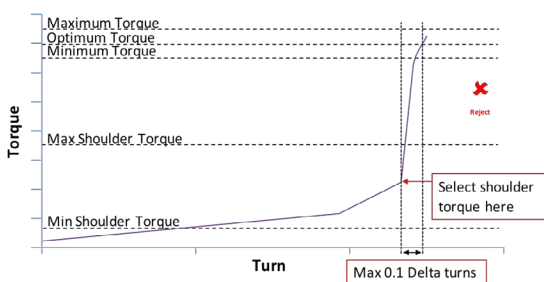


Figure 11.6.4 – Example of an unacceptable JFEBEAR make-up graph (loss of linearity falls out of the 0.1 delta turns criteria). *If in doubt, please contact your local JFE Technical Center*



Possible causes of the unacceptable graph profile but not limited to, are as follows:

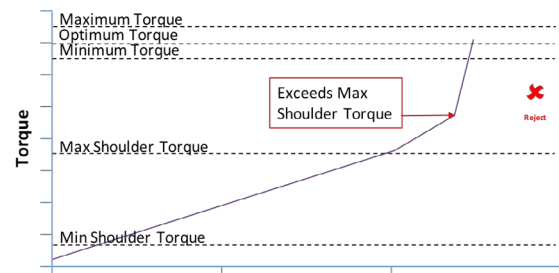
- Shoulder torque has not been selected correctly
- Dope is contaminated
- Pin or box dimensions are out with the tolerance range
- The surface treatment for the pin or box is out with the tolerance range
- Friction factor of dope is too low
- Load cell error

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists

It should be noted that if the delta turns are greater than 0.1, however no loss of linearity exists, the graph can be accepted.

Figure 11.6.5 – Example of an unacceptable JFEBEAR make up graph (Exceeds Max Shoulder Torque)



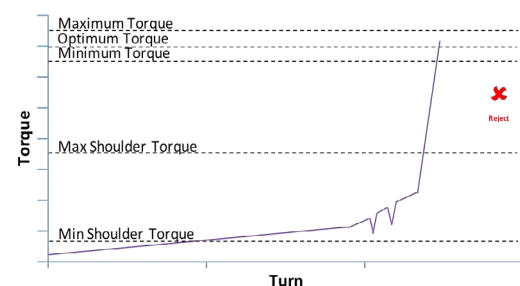
Possible causes of the unacceptable graph profile but not limited to, are as follows:

- Friction factor of dope is too high
- Dope is contaminated
- Pipe may not be straight
- Pin or box dimensions are out with the tolerance range
- The surface treatment for the pin or box is out with the tolerance range

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists

Figure 11.6.6 – Example of an unacceptable JFEBEAR make up graph (Slipping during seal engagement portion)



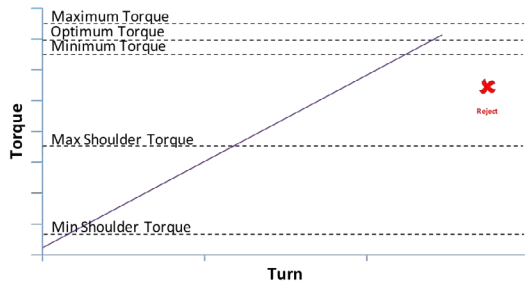
Possible causes of the unacceptable graph profile but not limited to, are as follows:

- Pipe may not be straight
- Jaw of power tong is worn out or dirty

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists

Figure 11.6.7 – Example of an unacceptable JFEBEAR make up graph (No clear shoulder torque)



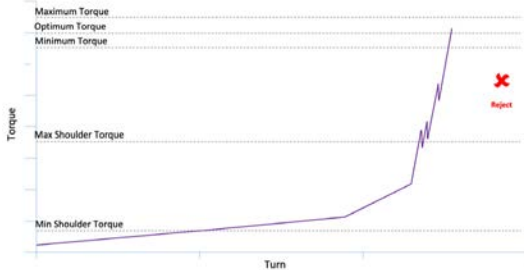
Possible causes of the unacceptable graph profile but not limited to, are as follows:

- Friction factor of dope is too high
- Dope is contaminated
- Pipe may not be straight
- Pin or box dimensions are out with the tolerance range

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists

Figure 11.6.8 – Example of an unacceptable make up graph (Slipping after shouldering)



Possible causes of the unacceptable graph profile but not limited to, are as follows:

- Jaw of power tong is worn
- Contamination on pipe/coupling or dies/jaw
- Gripping pressure too low

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Determine the root cause of slippage
- Re-make up if no galling exists

Figure 11.6.9 – Example of an acceptable JFEBEAR make-up graph (the maximum torque value of the dope hump exceeds the maximum shoulder torque, however linearity is re-established prior to shouldering at a value below maximum shoulder torque)

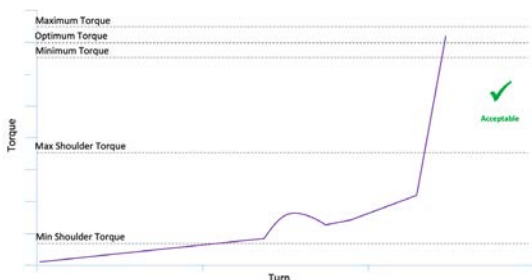


Figure 11.6.10 – Example of an acceptable JFEBEAR make-up graph (shoulder torque and maximum torque value of the dope hump are below maximum shoulder torque where dope hump extends into shoulder torque gradient)

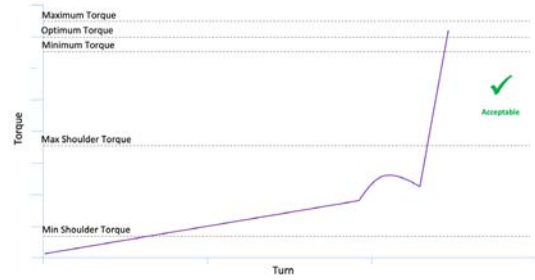


Figure 11.6.11 – Example of an unacceptable JFEBEAR make-up graph (the maximum torque value of the dope hump exceeds the maximum shoulder torque, however linearity is re-established prior to shouldering at a value below maximum shoulder torque)

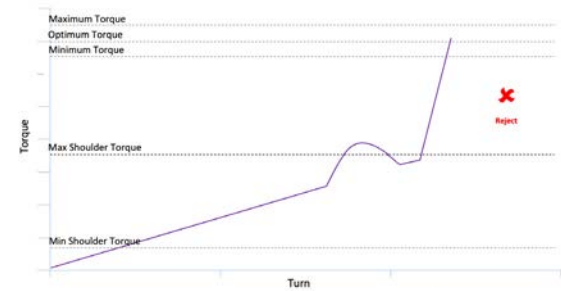
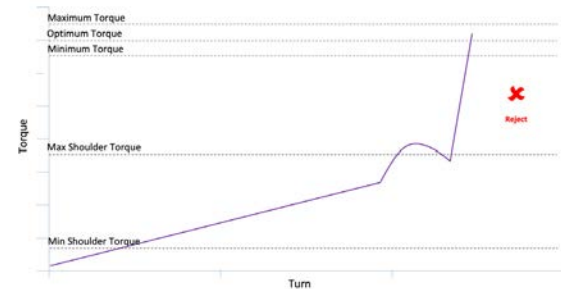


Figure 11.6.12 – Example of an unacceptable JFEBEAR make-up graph (the peak torque value of the dope hump is above the maximum shoulder torque value and the selected position is within the dope hump area)



Possible causes of the unacceptable graph profile but not limited to, are as follows:

- Dope is contaminated
- Excessive dope application

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists

Size (inch)	Weight (lb/ft)	Pipe Body Wall (inch)	80,85,90,95 ksi				
			Final Torque			Shoulder Torque	
			Minimum	Optimum	Maximum	Minimum	Maximum
7	29.00	0.408	N/A				
	32.00	0.453	N/A				

Size (inch)	Weight (lb/ft)	Pipe Body Wall (inch)	110 ksi (P110) Grade Torque (ft-lb)				
			Final Torque			Shoulder Torque	
			Minimum	Optimum	Maximum	Minimum	Maximum
7	29.00	0.408	37,000	39,000	41,000	2,730	25,350
	32.00	0.453	40,500	42,500	44,500	2,975	27,625

Size (inch)	Weight (lb/ft)	Pipe Body Wall (inch)	125 ksi (P110 CY) Grade Torque (ft-lb)				
			Final Torque			Shoulder Torque	
			Minimum	Optimum	Maximum	Minimum	Maximum
7	29.00	0.408	42,500	44,500	46,500	3,115	28,925
	32.00	0.453	46,500	48,500	50,500	3,395	31,525

Size (inch)	Weight (lb/ft)	Pipe Body Wall (inch)	80,85 ksi Grade Torque (ft-lb)				
			Final Torque			Shoulder Torque	
			Minimum	Optimum	Maximum	Minimum	Maximum
3.250	6.60	0.200	2,160	2,400	2,640	360	1,920

Size (inch)	Weight (lb/ft)	Pipe Body Wall (inch)	80,85 ksi Grade Torque (ft-lb)				
			Final Torque			Shoulder Torque	
			Minimum	Optimum	Maximum	Minimum	Maximum
3.250	6.60	0.200	3,240	3,800	4,180	570	3,040

Size (inch)	Weight (lb/ft)	Pipe Body Wall (inch)	80,85 ksi Grade Torque (ft-lb)				
			Final Torque			Shoulder Torque	
			Minimum	Optimum	Maximum	Minimum	Maximum
3.250	6.60	0.200	2,790	3,100	3,410	465	2,480

It is recommended to check the following website for up to date torque information: www.jfetc.com

11.8 Hydrostatic Test Fixtures

JFEBEAR Hydrostatic test fixtures are low torque, however require metal to metal seal contact to achieve a pressure test. Soft seal options are currently not available.

The following points shall be noted when manufacturing JFEBEAR Test Caps and Plugs:

- The following information shall be low stress stamped on all test fixtures. Size, Weight, and Maximum Working Pressure, the maximum pressure shall not exceed 10,000psi.

Example: 3.5" All weights JFEBEAR P110 MWP = 10,000psi

- Test caps and plugs shall be manufactured from low alloy steel with a minimum yield strength of 110ksi and maximum yield strength of 140ksi.
- Higher rated Autoclave connections can be used instead of 1/2" NPT. But the maximum working pressure will remain limited to 10,000psi unless otherwise specified by the controlling center.

11.8.1 Make-up of JFEBEAR Hydrostatic Cap or Plug

Only low torque is required to engage the seal for testing, therefore the test cap or plug should not be made up with a power unit.

For caps or plugs that do not have handles installed a strap/chain wrench should be used after hand tightening to assure seal engagement.

For cap or plugs that have handles installed, hand tightening with the handles should be sufficient. If not a cheater bar positioned over the handle can be used to further engage the seals.

JFE do not advise the use of any type of seal rings during pressure testing.

11.8.2 Storage and Maintenance

After use, the fixtures should be thoroughly cleaned and inspected for any damage that may have occurred during assembly. The connection should be dried and a suitable storage compound such as Kendex applied prior to installation of thread protectors. It is recommended that the fixtures be stored indoors and are not subjected to outdoor weather conditions.

It is recommended to perform NDE on the entire body of the fixture annually to check for any surface breaking and or sub-surface defects such as cracks.

11.8.3 Disclaimer

The users of these test caps and plugs are liable for the maintenance, use and safe operation. In no event shall JFE be liable for any damages, costs and expenses incurred in connection with the use of these test fixtures.

11.9 End Finishing Requirements

11.9.1 JFEBEAR Standard End Finishing Requirements

OD (inch)	High Chrome ¹ Steel Pin End Finish	High Chrome ¹ Steel Box End Finish	Carbon Steel Pin End Finish	Carbon Steel Box End Finish
2 3⁄8 – 4 1⁄2	Bead Blast Mill & Field End	Copper-Plate or Clear-Plate™	Bead Blast Mill & Field End	Manganese Phosphate or Clear-Plate™
5 – 9 5⁄8			Bare or Bead Blast Mill & Field End	

11.9.2 JFEBEAR Clear Run End Finishing Requirements

OD (inch)	High Chrome ¹ Steel Pin End Finish	High Chrome ¹ Steel Box End Finish	Carbon Steel Pin End Finish	Carbon Steel Box End Finish
2 3⁄8 – 6 5⁄8	Bead Blast Mill & Field End	Clear-Plate™	Bead Blast Mill & Field End	Manganese Phosphate
7 – 9 5⁄8			Bare or Bead Blast Mill & Field End	Clear-Plate™
7 HTP	Not applicable		Bead Blast Mill & Field End	

Note¹ - Definition of high chrome steel: Containing ≥ 9%Cr



An example of a JFEBEAR coupling where Clear-Plate™ has been applied as the end finish

11.10 Special clearance OD dimensions

JFEBEAR Special Clearance Coupling OD's					
Size (inch)	Weight (lb/ft)	Wall Thickness (inch)	SC80 (inch)	SC90 (inch)	Tolerance (inch)
2 3⁄8	4.60	0.190	2.621	2.652	
	5.80	0.254	2.695	2.735	
	6.60	0.295	2.739	2.784	
	7.35	0.336	2.781	2.830	
2 7⁄8	6.40	0.217	3.140	3.176	
	7.80	0.276	3.211	3.255	
	8.60	0.308	3.247	3.295	
	9.35	0.340	3.282	3.334	
	10.50	0.392	3.336	3.394	
	11.50	0.440	3.383	3.445	
3 1⁄2	7.70	0.216	3.743	3.781	
	9.20	0.254	3.792	3.836	
	10.20	0.289	3.836	3.884	
	12.70	0.375	3.936	3.995	
	14.30	0.430	3.996	4.061	
	15.50	0.476	4.043	4.114	
	17.00	0.530	4.096	4.172	
	9.50	0.226	4.241	4.281	
4	10.70	0.262	4.288	4.334	
	11.60	0.286	4.319	4.368	
	13.20	0.330	4.374	4.429	
	14.80	0.380	4.434	4.495	
	16.10	0.415	4.474	4.540	
4 1⁄2	11.60	0.250	4.778	4.822	
	12.60	0.271	4.806	4.853	
	13.50	0.290	4.831	4.881	
	15.20	0.337	4.891	4.948	
	17.00	0.380	4.944	5.007	
	18.90	0.430	5.003	5.073	
	21.50	0.500	5.082	5.160	
	23.70	0.560	5.147	5.232	
	13.00	0.253	5.273	5.318	
	15.00	0.296	5.331	5.383	
5	18.00	0.362	5.416	5.478	
	21.40	0.437	5.508	5.580	
	23.20	0.478	5.557	5.634	
	24.10	0.500	5.582	5.662	
5 1⁄2	15.50	0.275	5.806	5.855	+ 0.020 / - 0
	17.00	0.304	5.845	5.899	
	20.00	0.361	5.920	5.982	
	23.00	0.415	5.988	6.058	
	26.00	0.476	6.063	6.141	
	26.80	0.500	6.091	6.173	
6	24.10	0.400	6.472	6.541	
6 5⁄8	20.00	0.288	6.942	6.995	
	24.00	0.352	7.030	7.092	
	28.00	0.417	7.116	7.188	
7	32.00	0.475	7.190	7.271	
	23.00	0.317	7.347	7.404	
	26.00	0.362	7.409	7.473	
	29.00	0.408	7.470	7.542	
	32.00	0.453	7.529	7.607	
	35.00	0.498	7.587	7.672	
	38.00	0.540	7.639	7.730	
	42.70	0.625	7.743	7.845	
7 5⁄8	46.40	0.687	7.815	7.925	
	29.70	0.375	8.043	8.111	
	33.70	0.430	8.118	8.193	
	39.00	0.500	8.209	8.296	
	42.80	0.562	8.288	8.384	
	45.30	0.595	8.329	8.429	
7 3⁄4	47.10	0.625	8.366	8.470	
	46.10	0.595	8.456	8.556	
	32.00	0.352	9.016	9.080	
	36.00	0.400	9.082	9.155	
8 5⁄8	40.00	0.450	9.151	9.231	
	44.00	0.500	9.217	9.305	
	49.00	0.557	9.292	9.388	
9 5⁄8	36.00	0.352	10.019	10.084	
	40.00	0.395	10.079	10.151	
	43.50	0.435	10.135	10.214	
	47.00	0.472	10.186	10.270	
	53.50	0.545	10.284	10.380	
	58.40	0.595	10.350	10.453	
	59.40	0.609	10.368	10.473	



12.1 Design Features

Figure 12.1.1 – Box Detail



Figure 12.1.2 – Pin Detail



Figure 12.1.3 – Pin Detail with swage



OD (inch)	Threads per Inch (TPI)
7 to 9 5/8	5
9 7/8"	4

12.2 Interchangeability

JFETIGER connections with differing weights are interchangeable within a given OD. Rules when mixing differing weights & grades:

- The lower make-up torque of the lighter weight/lower grade connection should be used
- If pin weight is heavier, a step will extrude into pipe bore from pin
- If box weight is heavier, a step will extrude into pipe bore from box
- Couplings with differing weights may have differing OD's

The following tables provide examples of the rules when mixing various weights and grades for JFETIGER.

Figure 12.2.1 – Differing Weights + Identical Grades (ID step = 0.031", Applied torque is the lesser torque value of the combined connections.)

3 1/2" JFETIGER	Weight	Grade	Nominal Connection ID	Minimum Field Torque	Optimum Field Torque	Maximum Field Torque
	lb/ft	ksi	inch	ft-lb		
Box	10.2	80	2.915	4040	4490	4940
Pin	12.7	80	2.853	4710	5230	5760
				Applicable Torque		
Step/side (inch)			0.031	4040	4490	4940

Figure 12.2.2 – Identical Weights + Differing Grades (No ID step, Applied torque is the lesser torque value of the combined connections.)

3 1/2" JFETIGER	Weight	Grade	Nominal Connection ID	Minimum Field Torque	Optimum Field Torque	Maximum Field Torque
	lb/ft	ksi	inch	ft-lb		
Box	10.2	80	2.915	4040	4490	4940
Pin	10.2	95	2.915	4690	5210	5730
				Applicable Torque		
Step/side (inch)			0	4040	4490	4940

Figure 12.2.3 – Differing Weights + Differing Grades (ID step = 0.042", Applied torque is the lesser torque value of the combined connections.)

4 1/2" JFETIGER	Weight	Grade	Nominal Connection ID	Minimum Field Torque	Optimum Field Torque	Maximum Field Torque
	lb/ft	ksi	inch	ft-lb		
Box	15.2	95	3.852	7110	7900	8690
Pin	12.6	80	3.936	4860	5400	5940
				Applicable Torque		
Step/side (inch)			0.042	4860	5400	5940

12.3 Field Inspection

Field Inspection Tools

The following tools are commonly used but not limited to during field inspection & repair procedures:

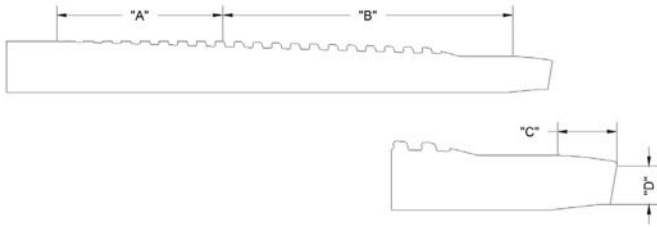
- Depth Gauge
- Fine Tooth Triangle File
- Scotch Brite
- Emery Cloth
- Soft Stone
- Vernier Calipers
- Rotary Tools¹

¹ Rotary tools can only be used by qualified JFE field service personnel.

A selection of field repair tools are shown in the image below.



12.3.1 JFETIGER Pin Visual Inspection Criteria & Guidelines



Condition: Corrosion

Zone	Criteria	Action
A, B, D	All surfaces. Pitting less than 0.004" (0.1mm) deep or minor surface corrosion	Hand repair with soft bristle (no steel wire) brush or emery cloth
	Deeper than 0.004" (0.1mm)	Cut off & re-thread
C	No pitting acceptable	If present, cut off & re-thread
	Light surface corrosion (rust)	Hand repair with scotch brite or #400 emery cloth. Do not alter seal dimension. Repair should be made in a larger area than actual surface corrosion and should move around the circumference of the seal

Condition: Burr, Tear, Ding, Mash, Scratch

Zone	Criteria	Action
A, B, D	All surfaces. Any condition which could cause galling, i.e. conditions described greater than 0.010" (0.3mm).	Hand repair with a fine triangle file; emery cloth or rotary tool ¹ . Repair should be made in a larger area than actual effected area and should move around the helix of the thread. Otherwise - reject.
C	Not acceptable	If present, cut off & re-thread

Condition: Burnishing

Zone	Criteria	Action
C	Acceptable	On as-machined surfaces, burnishing from the thread protector may be evident. As long as this does not appear as a step, this is acceptable.

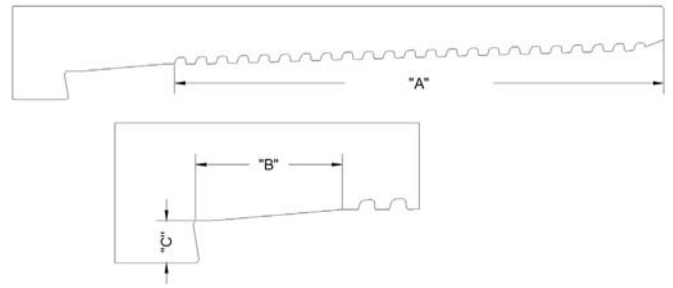
Condition: Bead Peening

Zone	Criteria	Action
A,B, C, D	Inspect for peened surface. If previously made-up, normal wear is expected and is acceptable	Bead peening is an optional end finish

Condition: Phosphate

Zone	Criteria	Action
A,B, C, D	Inspect for phosphate surface. If previously made-up, burnishing is expected and is acceptable	Phosphate is an optional end finish

12.3.2 JFETIGER Box Visual Inspection Criteria & Guidelines



Condition: Corrosion

Zone	Criteria	Action
A, C	Slight imperfections and light surface corrosion, i.e. Less than 0.004" (0.1mm)	Hand repair with soft bristle (no steel wire) brush, emery cloth or scotch brite
	All other imperfections deeper than 0.004" (0.1mm)	Reject or re-thread
B	No pitting acceptable	Reject or re-thread
	Light surface corrosion (rust)	Hand repair with scotch brite or #400 emery cloth. Do not alter seal dimension. Repair should be made in a larger area than actual surface corrosion and should move around the circumference of the seal
Coupling OD, ID Bore & Bearing Face	Pitting or corrosion less than 0.020" (0.5mm) deep	Grind to the bottom of the pit & smooth edges. Keep within product tolerances.
	Deeper than 0.020" (0.5mm)	Reject or re-thread

Condition: Burr, Tear, Ding, Mash, Scratch

Zone	Criteria	Action
A, C	All surfaces. Any condition which could cause galling, i.e. conditions described greater than 0.010" (0.3mm)	Hand repair with a honing stone / small file; emery cloth or rotary tool ¹ . Repair should be made in a larger area than actual effected area and should move around the helix of the thread. Otherwise - reject.
B	Not acceptable	Reject or re-thread

Condition: Manganese phosphate

Zone	Criteria	Action
A, B, C	Must be present. Inspect for medium grey surface color. If previously made-up, normal wear is expected and is acceptable	Manganese phosphate if not present, reject, or re phosphate

Condition: Copper-plate and Clear-Plate™

Zone	Criteria	Action
A, B, C	Inspect the electroplated surface. Oxidation or discolouration of the plated surface is acceptable. If previously made-up, normal wear is expected and acceptable. Any delamination of plating is cause for reject	If holiday/delamination exists, reject or re-plate

12.4 Approved Thread Compounds

This procedure recommends the thread compounds that can be used to make-up JFE connections.

JFE do not recommend the use of thread compounds containing PTFE (Teflon®) for premium connections.

List of Approved Thread Compounds include, but are not limited to:

JFETIGER Approved Thread Compounds

Connection	Material Grade	API Modified [1]	Weatherford Lube Seal	Jet-Lube HPHT
JFETIGER®	Carbon	✓	✓	✗
	9Cr to 17Cr	✓	✓	✗
	CRA	✓	✓	✗

Connection	Material Grade	BOL 4010NM	TOPCO Green Seal II	Clear-Glide™ [2]	BOL 2000
JFETIGER®	Carbon	✓	✗	[3]	✗
	9Cr to 17Cr	[4]	✗	[3]	✗
	CRA	[4]	✗	[3]	✗

[1] Thread compounds that are in compliance with API RP 5A3 Annex A can be used on JFE connections. Different names are given and are dependent on the thread compound manufacturer.

[2] Clear-Glide™ is to be used only with Clear-Run™ prepared tubulars, i.e. when the proper end finishing is applied.

[3] Contact your local JFETC office for further information.

[4] Can be applied to sizes larger than 5.5" with Mn phosphate on the couplings, if the pin ends are abrasive blasted in accordance with JFE specifications.

JFE continues to evaluate the use of thread compounds. It is recommended to contact your nearest JFE-TC office for further information if other compounds that are not listed are required. Please continuously refer to www.jfetc.com for the most updated list and technical data.

This table is for informational purpose only.

12.5 Lifting Plugs

Figure 12.5.1 – Example of main body for lift plug (seal removed)



The following points shall be adhered to for JFETIGER lift plugs:

- The lift plug shall be manufactured from low alloy steel with a specified minimum yield stress (SMYS) of 110ksi, and a maximum yield stress of 140ksi.
- The lift plug shall be bead peened, phosphated or copper-plated as per the relevant procedures. Once machining has been completed, weld on handles can be installed to assist with handling and assembling operations. If handles are installed, they shall be of appropriate size and orientated 0° and 180°.
- The lift plug is low torque and therefore a power tong is not required. Final positioning before lifting operation can be achieved using the handles or strap wrench/chain tong

The following information shall be low stress stamped on the lift plug where drifting operations are not required:

Size, All weights, grade and JFETIGER Lift Plug
Licensee code plus manufacturing date
For lifting a maximum of three joints only

Stencil Example

9 5/8" All weights AISI 4145 110ksi JFETIGER Lift Plug
SI-081; 22nd April 2021
For lifting a maximum of three joints only

The following information shall be low stress stamped on the lift plug where drifting through the plug is required:

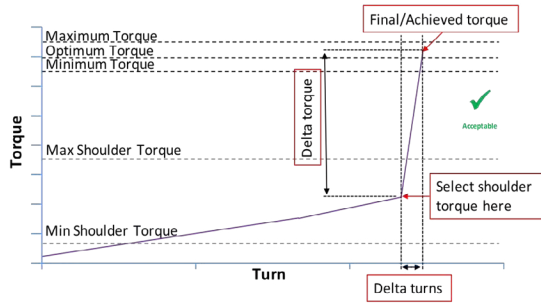
Size, weight, grade and JFETIGER Lift Plug
Bore ID = XXXX
Licensee code plus manufacturing date
For lifting a maximum of three joints only

Example

7" 32# AISI 110ksi JFETIGER Lift Plug
Bore ID = 6.094"
SI-081; 22nd April 2021
For lifting a maximum of three joints only

12.6 Make-Up Acceptance Criteria

Figure 12.6.1 – Example of an acceptable, typical JFELION/JFETIGER make up graph



If a case exists where premature dump torque occurs or a high shoulder is observed, if:

Achieved delta torque = minimum torque – maximum shoulder

the graph may be accepted. This rule can be applied for standalone cases, however if high shoulders continue to occur/premature dump occurs, contact your local JFE-TC office for further advice.

Figure 12.6.2 – Example of an acceptable JFELION/JFETIGER make-up graph (shoulder torque and maximum torque value of the dope hump are below maximum shoulder torque and linearity is re-established prior to shouldering)

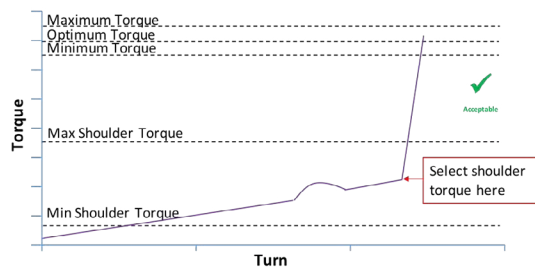


Figure 12.6.3 – Example of an acceptable JFELION/JFETIGER make-up graph (the maximum torque value of the dope hump does not exceed the maximum shoulder torque, and the dope hump extends immediately into the shoulder torque point).

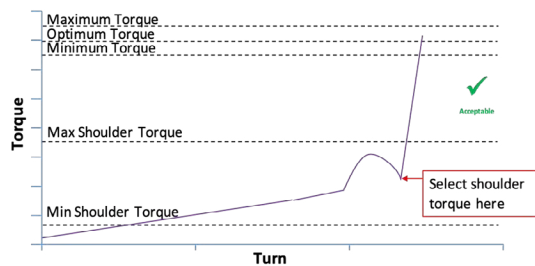


Figure 12.6.4 – Example of an acceptable JFELION/JFETIGER make-up graph (minor loss of linearity within 0.1 delta turns). If delta turns are higher than 0.1, however the graph remains linear, the graph is acceptable.

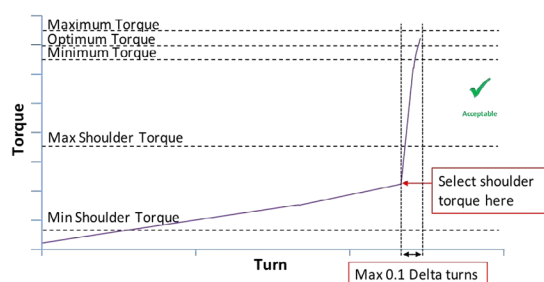
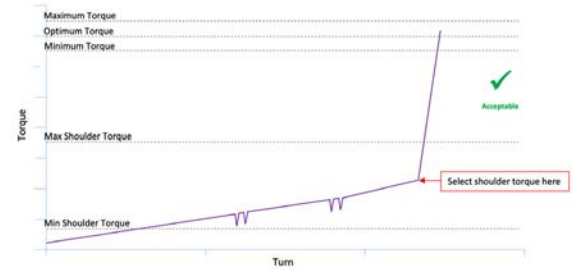


Figure 12.6.5 – Example of an acceptable JFELION/JFETIGER make-up graph. Minor slippage during thread engagement and slope returns to similar gradient once slipping occurs. Rectify for next make-up



Possible causes of graph profile but not limited to, are as follows:

- Pipe may not be straight
- Jaw of power tong is worn out or dirty

Figure 12.6.6 – Example of an unacceptable JFELION/JFETIGER make-up graph (the maximum torque value of the dope hump exceeds the maximum shoulder torque, however linearity is re-established prior to shouldering at a value below maximum shoulder torque)

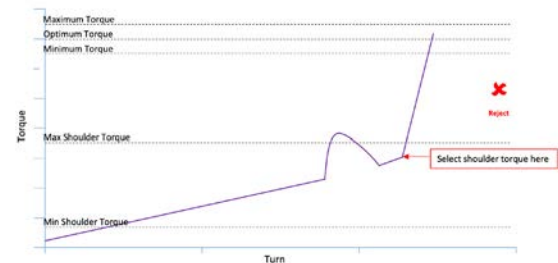
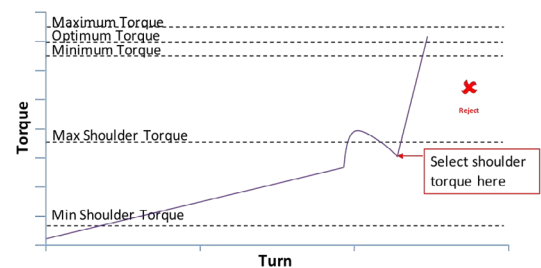


Figure 12.6.7 – Example of an unacceptable JFELION/JFETIGER make-up graph (the peak torque value of the dope hump is above the maximum shoulder torque value and the selected position is within the dope hump area)



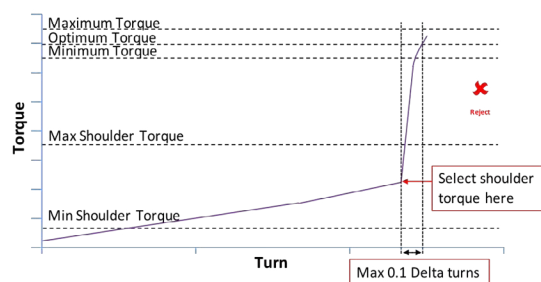
Possible causes of unacceptable graph profile but not limited to, are as follows:

- Dope is contaminated
- Excessive dope application

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists

Figure 12.6.8 – Example of an unacceptable JFELION/JFETIGER make-up graph (loss of linearity falls out of the 0.1 delta turns criteria). If in doubt, please contact your local JFE Technical Center



Possible causes of unacceptable graph profile but not limited to, are as follows:

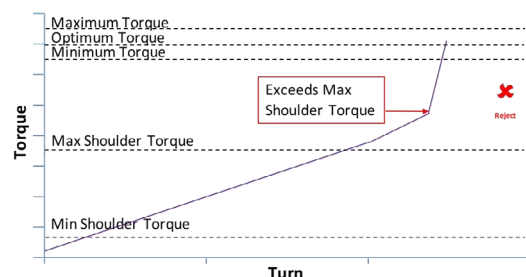
- Dope is contaminated
- Pin or box dimensions are out with the tolerance range
- The surface treatment for the pin or box is out with the tolerance range
- Friction factor of dope is too low
- Load cell error

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Check for deformed torque shoulder and if deformation is evident, lay down both pin and box
- Re-make up if no galling exists

It should be noted that if the delta turns are greater than 0.1, however no loss of linearity exists, the graph can be accepted

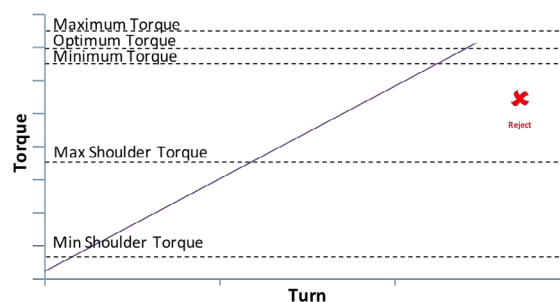
Figure 12.6.9 – Example of an unacceptable JFELION/JFETIGER make up graph (Exceeds Max Shoulder Torque)



Possible causes of unacceptable graph profile but not limited to, are as follows:

- Friction factor of dope is too high
- Pipe may not be straight
- Pin or box dimensions are out with the tolerance range
- The surface treatment for the pin or box is out with the tolerance range
- Procedure if the above graph profile is encountered:
- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists

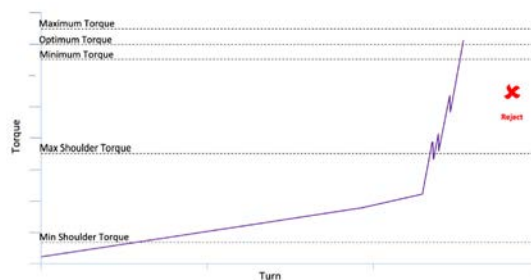
Figure 12.6.10 – Example of an unacceptable JFELION/JFETIGER make up graph (Exceeds Max Shoulder Torque)



Possible causes of unacceptable graph profile but not limited to, are as follows:

- Friction factor of dope is too high
- Dope is contaminated
- Pipe may not be straight
- Pin or box dimensions are out with the tolerance range
- The surface treatment for the pin or box is out with the tolerance range
- Procedure if the above graph profile is encountered:
- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists

Figure 12.6.11 – Example of graph where unacceptable slippage has occurred after shouldering



Possible causes of unacceptable graph profile but not limited to, are as follows:

- Jaw of power tong is worn
- Contamination on pipe/coupling or dies/jaw
- Gripping pressure too low

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Determine the root cause of slippage
- Re-make up if no galling exists

12.8 End Finishing Requirements

OD (inch)	High Chrome ¹ Steel Pin End Finish	High Chrome ¹ Steel Box End Finish	Carbon Steel Pin End Finish	Carbon Steel Box End Finish
All	Bead Blast Mill & Field End	Clear-Plate™ ²	Bead Blast Mill & Field End	Manganese Phosphate or Clear-Plate™ ³

Note¹ - Definition of high chrome steel: Containing ≥ 9%Cr

Note² - Copper-plate is applicable to accessories, however dry lubricant spray containing Molybdenum disulphide shall be sprayed over the seal and shoulder area for anti-galling. This shall be approved by JFE-TC prior to make-up.

Note³ - Clear-Plate™ is mandatory when being used within the Clear Run™ system and blasting is not required prior to Clear-Plate. API modified can also be used in conjunction with Clear-Plate™ where there will be no change to the friction factor (FF).

12.9 Special Clearance OD Dimensions

It is recommended to use slip type elevators for special clearance OD couplings.

JFETIGER Special Clearance Coupling OD's					
Size (inch)	Weight (lb/ft)	Wall Thickness (inch)	SC80 (inch)	SC90 (inch)	Tolerance (inch)
7	23.00	0.317	7.602	7.658	+ 0.020 / - 0
	26.00	0.362	7.651	7.714	
	29.00	0.408	7.676	7.746	
	32.00	0.453	7.676	7.753	
	35.00	0.498	7.730	7.814	
	38.00	0.540	7.766	7.856	
7 5⁄8	29.70	0.375	8.212	8.278	
	33.70	0.430	8.269	8.343	
	39.00	0.500	8.331	8.416	
	42.80	0.562	8.385	8.479	
	45.30	0.595	8.430	8.528	
	47.10	0.625	8.471	8.574	
8 5⁄8	40.00	0.450	9.407	9.485	
	44.00	0.500	9.391	9.477	
	49.00	0.557	9.482	9.577	
	52.00	0.595	9.542	9.641	
	54.00	0.625	9.588	9.691	
	57.40	0.656	9.635	9.743	
	58.70	0.687	9.682	9.794	
9 5⁄8	59.20	0.700	9.702	9.816	
	40.00	0.395	10.345	10.415	
	43.50	0.435	10.331	10.408	
	47.00	0.472	10.354	10.438	
	53.50	0.545	10.437	10.531	
	58.40	0.595	10.453	10.556	
	59.40	0.609	10.473	10.578	
9 7⁄8	62.80	0.625	10.852	10.958	
	65.30	0.650	10.844	10.954	
	66.40	0.661	10.841	10.952	
	66.90	0.668	10.838	10.951	
	67.50	0.678	10.835	10.950	
	68.00	0.694	10.830	10.947	
	68.90	0.700	10.828	10.946	



13.1 Design Features

Figure 13.1.1 – Box Detail



Figure 13.1.2 – Pin Detail



Figure 13.1.3 – Pin Detail with swage



OD (inch) & Classification Number	Threads per Inch (TPI)
2 7/8 to 2 7/8	8
3 1/2 to 5*	6
5 1/2 to 9 5/8	5
9 7/8 to 14	4

*4 1/2" SD 51 (21.5lb/ft & 23.7lb/ft) are 5 threads per inch

13.2 Interchangeability

Interchangeability rules for JFELION only apply to connections with identical SD number. If differing weights of the same diameter connection do not have the same SD number, the connections are not interchangeable.

Figure 13.2.1 – Example: JFELION 7" 23# SD49 & 7" 29# SD49 are interchangeable. JFELION 7" 23# SD49 is not interchangeable with 7" 32# SD52. The following table details the interchangeable weights within a given size for the JFELION connection.

OD (inch)	Classification / SD No.	Lower Weight (lb/ft)	Upper Weight (lb/ft)
2 7/8	SD26	6.4	6.4
	SD30	7.8	9.4
3 1/2	SD29	9.2	10.2
	SD35	12.7	14.8
4	SD35	11.6	16.1
4 1/2	SD29	11.6	12.6
	SD32	13.5	15.2
	SD35	17.0	18.9
	SD51	21.5	23.7
5	SD30	15.0	15.0
	SD36	18.0	21.4
	SD38	23.2	24.1
5 1/2	SD41	15.5	17.0
	SD46	20.0	23.0
	SD49	26.0	26.8
	SD51	28.4	29.7
6	SD45	22.8	22.8
	SD50	32.0	32.0
6.068	SD61	32.6	32.6
6 5/8	SD41	20.0	20.0
	SD49	24.0	32.0
	SD54	40.2	40.2

OD (inch)	Classification / SD No.	Lower Weight (lb/ft)	Upper Weight (lb/ft)
7	SD49	23.0	29.0
	SD52	32.0	35.0
	SD54	38.0	42.7
7 5/8	SD47	26.4	29.7
	SD52	33.7	39.0
	SD57	42.8	42.8
8 5/8	SD50	36.0	44.0
	SD57	49.0	52.0
	SD62	54.0	57.4
9 5/8	SD51	40.0	43.5
	SD57	47.0	59.4
9 7/8	SD68	62.8	68.9
10 3/4	SD56	51.0	51.0
	SD65	55.5	73.2
10 7/8	SD65	72.0	72.0
11 3/4	SD62	60.0	71.0
11 7/8	SD62	62.0	71.8
	SD63	68.0	77.0
13 3/8	SD65	80.7	86.0
	SD68	92.0	92.0
13 5/8	SD65	88.2	88.2
	SD66	93.0	93.0
14	SD68	100.0	115.0
9 5/8	CBR	53.5	53.5

Rules when mixing differing weights & grades:

- The lower make-up torque of the lighter weight / lower grade connection should be used
- If pin weight is heavier, a step will extrude into pipe bore from pin
- If box weight is heavier, a step will extrude into pipe bore from box
- Couplings with differing weights may have differing OD's
- JFELION CBR, & JFELION DR ASM do not offer interchangeability with any other connections

The following tables provide examples of the rules when mixing various weights (within the given SD number) and grades for the JFELION connection.

Figure 13.2.2 – Differing Weights + Identical SD# + Identical Grades (ID step = 0.0285", Applied torque is the lesser torque value of the combined connections.)

7" JFELION SD49	Weight	Grade	Nominal Connection ID	Minimum Field Torque	Optimum Field Torque	Maximum Field Torque
	lb/ft	ksi	inch	ft-lb		
Box	23.0	80	6.277	9900	11000	12100
Pin	29.0	80	6.220	13140	14600	16060
Applicable Torque						
Step/side (inch)		0.0285		9900	11000	12100

Figure 13.2.3 – Identical Weights + Identical SD# + Differing Grades (No ID step, Applied torque is the lesser torque value of the combined connections.)

7" JFELION SD49	Weight	Grade	Nominal Connection ID	Minimum Field Torque	Optimum Field Torque	Maximum Field Torque
	lb/ft	ksi	inch	ft-lb		
Box	29.0	80	6.220	13140	14600	16060
Pin	29.0	95	6.220	14040	15600	17160
Applicable Torque						
Step/side (inch)		0		13140	14600	16060

Figure 13.2.4 – Differing Weights + Identical SD# + Differing Grades (ID step: 0.0225", Applied torque is the lesser torque value of the combined connections.)

10.750" JFELION SD65	Weight	Grade	Nominal Connection ID	Minimum Field Torque	Optimum Field Torque	Maximum Field Torque
	lb/ft	ksi	inch	ft-lb		
Box	65.7	95	9.716	33750	37500	41250
Pin	60.7	80	9.840	26550	29500	32450
Applicable Torque						
Step/side (inch)		0.0285		26550	29500	32450

Note: These interchangeability rules are to be used when running tubing and casing. When assembling/ running accessories, it is recommended to contact your local JFE-TC office.

13.3 Field Inspection

Field Inspection Tools

The following tools are commonly used but not limited to during field inspection & repair procedures:

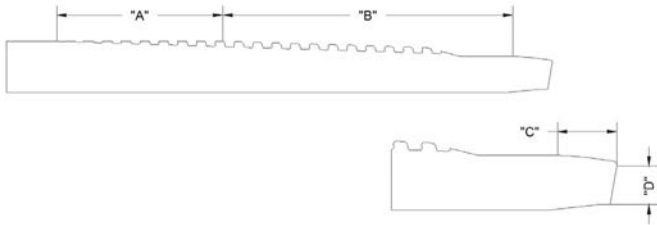
- Depth Gauge
- Fine Tooth Triangle File
- Scotch Brite
- Emery Cloth
- Soft Stone
- Vernier Calipers
- Rotary Tools¹

¹ Rotary tools can only be used by qualified JFE field service personnel.

A selection of field repair tools are shown in the image below.



13.3.1 JFELION Pin Visual Inspection Criteria & Guidelines



Condition: Corrosion

Zone	Criteria	Action
A, B, D	All surfaces. Pitting less than 0.004" (0.1mm) deep or minor surface corrosion	Hand repair with soft bristle (no steel wire) brush or emery cloth
	Deeper than 0.004" (0.1mm)	Cut off & re-thread
C	No pitting acceptable	If present, cut off & re-thread
	Light surface corrosion (rust)	Hand repair with scotch brite or #400 emery cloth. Do not alter seal dimension. Repair should be made in a larger area than actual surface corrosion and should move around the circumference of the seal

Condition: Burr, Tear, Ding, Mash, Scratch

Zone	Criteria	Action
A, B, D	All surfaces. Any condition which could cause galling, i.e. conditions described greater than 0.010" (0.3mm).	Hand repair with a fine triangle file; emery cloth or rotary tool ¹ . Repair should be made in a larger area than actual effected area and should move around the helix of the thread. Otherwise - reject.
C	Not acceptable	If present, cut off & re-thread

Condition: Burnishing

Zone	Criteria	Action
C	Acceptable	On as-machined surfaces, burnishing from the thread protector may be evident. As long as this does not appear as a step, this is acceptable.

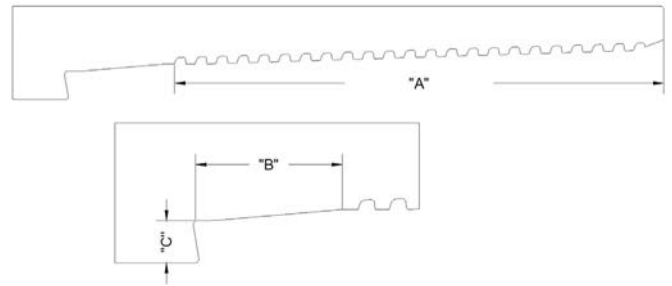
Condition: Bead Peening

Zone	Criteria	Action
A,B, C, D	Inspect for peened surface. If previously made-up, normal wear is expected and is acceptable	Bead peening is an optional end finish

Condition: Phosphate

Zone	Criteria	Action
A,B, C, D	Inspect for phosphate surface. If previously made-up, burnishing is expected and is acceptable	Phosphate is an optional end finish

13.3.2 JFELION Box Visual Inspection Criteria & Guidelines



Condition: Corrosion

Zone	Criteria	Action
A, C	Slight imperfections and light surface corrosion, i.e. Less than 0.004" (0.1mm)	Hand repair with soft bristle (no steel wire) brush, emery cloth or scotch brite
	All other imperfections deeper than 0.004" (0.1mm)	Reject or re-thread
B	No pitting acceptable	Reject or re-thread
	Light surface corrosion (rust)	Hand repair with scotch brite or #400 emery cloth. Do not alter seal dimension. Repair should be made in a larger area than actual surface corrosion and should move around the circumference of the seal
Coupling OD, ID Bore & Bearing Face	Pitting or corrosion less than 0.020" (0.5mm) deep	Grind to the bottom of the pit & smooth edges. Keep within product tolerances.
	Deeper than 0.020" (0.5mm)	Reject or re-thread

Condition: Burr, Tear, Ding, Mash, Scratch

Zone	Criteria	Action
A, C	All surfaces. Any condition which could cause galling, i.e. conditions described greater than 0.010" (0.3mm)	Hand repair with a honing stone / small file; emery cloth or rotary tool ¹ . Repair should be made in a larger area than actual effected area and should move around the helix of the thread. Otherwise - reject.
B	Not acceptable	Reject or re-thread

Condition: Manganese phosphate

Zone	Criteria	Action
A, B, C	Must be present. Inspect for medium grey surface color. If previously made-up, normal wear is expected and is acceptable	Manganese phosphate if not present, reject, or re phosphate

Condition: Copper-plate and Clear-Plate™

Zone	Criteria	Action
A, B, C	Inspect the electroplated surface. Oxidation or discolouration of the plated surface is acceptable. If previously made-up, normal wear is expected and acceptable. Any delamination of plating is cause for reject	If holiday/delamination exists, reject or re-plate

13.4 Approved Thread Compounds

This procedure recommends the thread compounds that can be used to make-up JFE connections.

JFE do not recommend the use of thread compounds containing PTFE (Teflon®) for premium connections.

List of Approved Thread Compounds include, but are not limited to:

JFELION Approved Thread Compounds

Connection	Material Grade	API Modified [1]	Weatherford Lube Seal	Jet-Lube HPHT
JFELION®	Carbon	✓	✓	✗
	9Cr to 17Cr	✓	✓	[8]
	CRA	✓	✓	[4]

Connection	Material Grade	BOL 4010NM	TOPCO Green Seal II	Clear-Glide™ [2]	BOL 2000
JFELION®	Carbon	≤5.5" [5][6]	[3]	[4]	✗
	9Cr to 17Cr	≤5.5" [7]	✗	[4]	✗
	CRA	≤5.5" [7]	✗	[4]	✗

[1] Thread compounds that are in compliance with API RP 5A3 Annex A can be used on JFE connections. Different names are given and are dependent on the thread compound manufacturer.

[2] Clear-Glide™ is to be used only with Clear-Run™ prepared tubulars, i.e. when the proper end finishing is applied.

[3] For use in geothermal well applications.

[4] Contact your local JFETC office for further information.

[5] Can be applied to sizes larger than 5.5" with as machined pins if Clear-Plate™ is applied to the coupling/box.

[6] Can be applied to sizes larger than 5.5" with Mn phosphate on the couplings, if the pin ends are abrasive blasted in accordance with JFE specifications.

[7] Can be applied to sizes larger than 5.5" if Clear-Plate™ is applied to the coupling/box.

JFE continues to evaluate the use of thread compounds. It is recommended to contact your nearest JFE-TC office for further information if other compounds that are not listed are required. Please continuously refer to www.jfetc.com for the most updated list and technical data.

This table is for informational purpose only.

13.5 Lifting Plugs

Figure 13.5.1 – Example of main body for lift plug (seal removed)



The following points shall be adhered to for JFELION lift plugs:

- The lift plug shall be manufactured from low alloy steel with a specified minimum yield stress (SMYS) of 110ksi, and a maximum yield stress of 140ksi.
- The lift plug shall be bead peened, phosphated or copper-plated as per the relevant procedures. Once machining has been completed, weld on handles can be installed to assist with handling and assembling operations. If handles are installed, they shall be of appropriate size and orientated 0° and 180°.
- The lift plug is low torque and therefore a power tong is not required. Final positioning before lifting operation can be achieved using the handles or strap wrench/chain tong

The following information shall be low stress stamped on the lift plug where drifting operations are not required:

Size, All weights, grade and JFELION Lift Plug
Licensee code plus manufacturing date
For lifting a maximum of three joints only

Stencil Example

9 5/8" 58.4# AISI 4145 110ksi JFELION SD57 Lift Plug
SI-081; 22nd April 2021

For lifting a maximum of three joints only

Note: 58.4# is stamped as this is the heaviest weight within the SD

The following information shall be low stress stamped on the lift plug where drifting through the plug is required:

Size, weight, grade JFELION SDXX Lift Plug
Bore ID = XXXX
Licensee code plus manufacturing date
For lifting a maximum of three joints only

Example

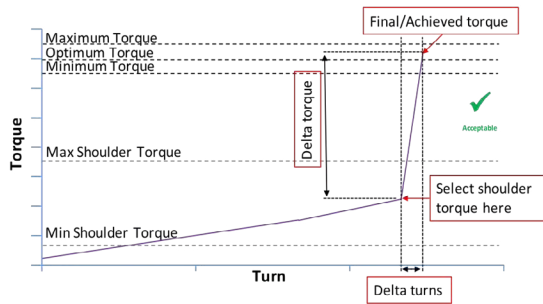
7" 29# AISI 110ksi JFELION SD49 Lift Plug
Bore ID = 6.184"

SI-081; 22nd April 2021

For lifting a maximum of three joints only

13.6 Make-Up Acceptance Criteria

Figure 13.6.1 – Example of an acceptable, typical JFELION/JFETIGER make up graph



If a case exists where premature dump torque occurs or a high shoulder is observed, if:

Achieved delta torque = minimum torque – maximum shoulder

the graph may be accepted. This rule can be applied for standalone cases, however if high shoulders continue to occur/premature dump occurs, contact your local JFE-TC office for further advice.

Figure 13.6.2 – Example of an acceptable JFELION/JFETIGER make-up graph (shoulder torque and maximum torque value of the dope hump are below maximum shoulder torque and linearity has since been re-established prior to shouldering)

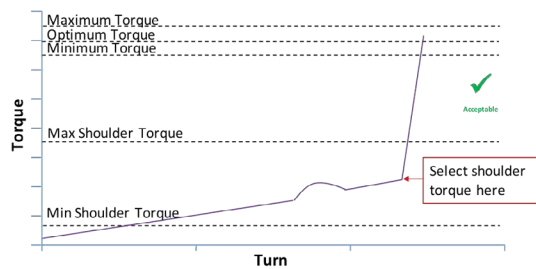


Figure 13.6.3 – Example of an acceptable JFELION/JFETIGER make-up graph (the maximum torque value of the dope hump does not exceed the maximum shoulder torque, and the dope hump extends immediately into the shoulder torque point).

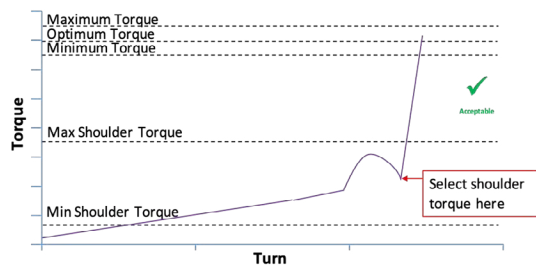


Figure 13.6.4 – Example of an acceptable JFELION/JFETIGER make-up graph (minor loss of linearity within 0.1 delta turns). If delta turns are higher than 0.1, however the graph remains linear, the graph is acceptable.

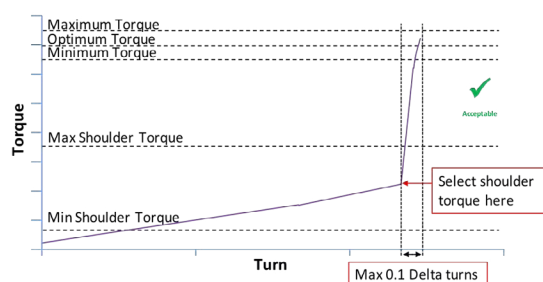
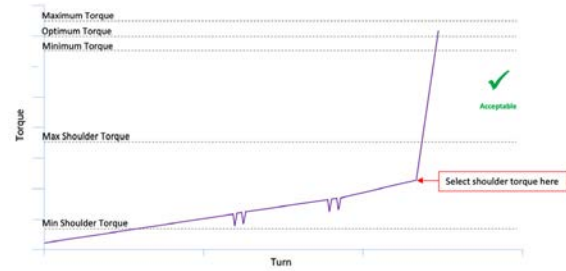


Figure 13.6.5 – Example of an acceptable JFELION/JFETIGER make-up graph. Minor slippage during thread engagement and slope returns to similar gradient once slipping occurs. Rectify for next make-up



Possible causes of graph profile but not limited to, are as follows:

- Pipe may not be straight
- Jaw of power tong is worn out or dirty

Figure 13.6.6 – Example of an unacceptable JFELION/JFETIGER make-up graph (the maximum torque value of the dope hump exceeds the maximum shoulder torque, however linearity is re-established prior to shouldering at a value below maximum shoulder torque)

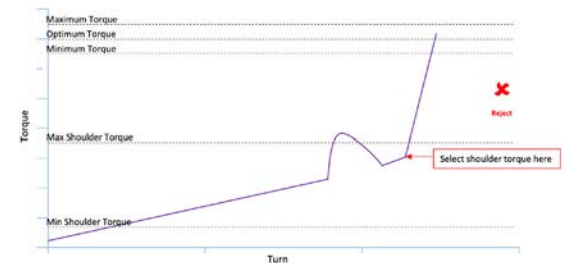
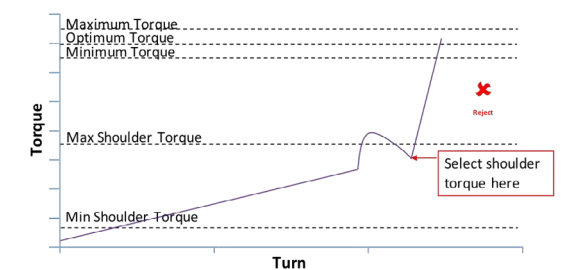


Figure 13.6.7 – Example of an unacceptable JFELION/JFETIGER make-up graph (the peak torque value of the dope hump is above the maximum shoulder torque value and the selected position is within the dope hump area)



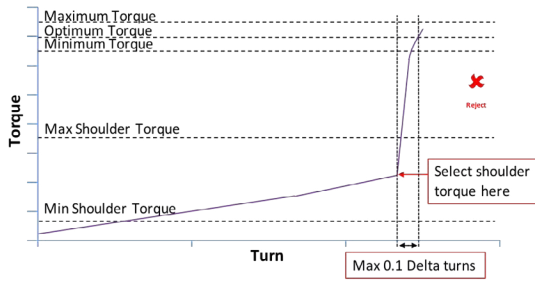
Possible causes of unacceptable graph profile but not limited to, are as follows:

- Dope is contaminated
- Excessive dope application

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists

Figure 13.6.8 – Example of an unacceptable JFELION/JFETIGER make-up graph (loss of linearity falls out of the 0.1 delta turns criteria). If in doubt, please contact your local JFE Technical Center



Possible causes of unacceptable graph profile but not limited to, are as follows:

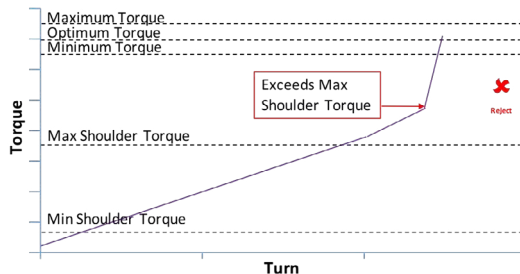
- Dope is contaminated
- Pin or box dimensions are out with the tolerance range
- The surface treatment for the pin or box is out with the tolerance range
- Friction factor of dope is too low
- Load cell error

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Check for deformed torque shoulder and if deformation is evident, lay down both pin and box
- Re-make up if no galling exists

It should be noted that if the delta turns are greater than 0.1, however no loss of linearity exists, the graph can be accepted

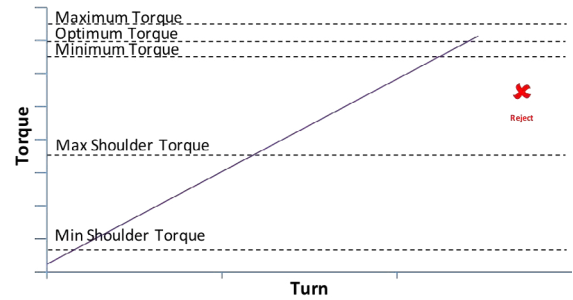
Figure 13.6.9 – Example of an unacceptable JFELION/JFETIGER make-up graph (Exceeds Max Shoulder Torque)



Possible causes of unacceptable graph profile but not limited to, are as follows:

- Friction factor of dope is too high
- Pipe may not be straight
- Pin or box dimensions are out with the tolerance range
- The surface treatment for the pin or box is out with the tolerance range
- Procedure if the above graph profile is encountered:
- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists

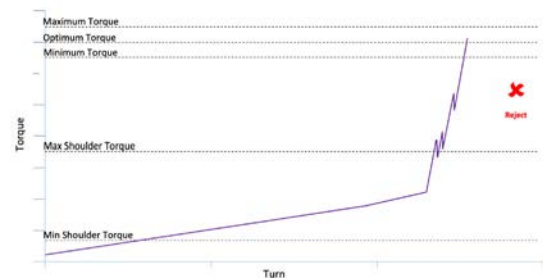
Figure 13.6.10 – Example of an unacceptable JFELION/JFETIGER make-up graph (Exceeds Max Shoulder Torque)



Possible causes of unacceptable graph profile but not limited to, are as follows:

- Friction factor of dope is too high
- Dope is contaminated
- Pipe may not be straight
- Pin or box dimensions are out with the tolerance range
- The surface treatment for the pin or box is out with the tolerance range
- Procedure if the above graph profile is encountered:
- Break-out, clean and inspect the connection
- Investigate the other components if connection looks OK
- Re-make up if no galling exists

Figure 13.6.11 – Example of graph where unacceptable slippage has occurred after shouldering



Possible causes of unacceptable graph profile but not limited to, are as follows:

- Jaw of power tong is worn
- Contamination on pipe/coupling or dies/jaw
- Gripping pressure too low

Procedure if the above graph profile is encountered:

- Break-out, clean and inspect the connection
- Determine the root cause of slippage
- Re-make up if no galling exists

Connection	Size (inch)	Weight (lb/ft)	Pipe Body Wall (inch)	80, 85 ksi Grade Torque (ft-lb)				
				Final Torque			Shoulder Torque	
				Min	Opt	Max	Min	Max
JFELION CBR	9 $\frac{5}{8}$	53.5	0.545	-	-	-	-	-
JFELION DR ASM	10 $\frac{3}{4}$	85.3	0.797	42,390	47,100	51,810	4,710	35,325
JFELION DR SS	10 $\frac{1}{8}$	79.3	0.795	44,100	49,000	53,900	4,900	36,740

Connection	Size (inch)	Weight (lb/ft)	Pipe Body Wall (inch)	90, 95 ksi Grade Torque (ft-lb)				
				Final Torque			Shoulder Torque	
				Min	Opt	Max	Min	Max
JFELION CBR	9 $\frac{5}{8}$	53.5	0.545	-	-	-	-	-
JFELION DR ASM	10 $\frac{3}{4}$	85.3	0.797	47,070	52,300	57,530	5,230	39,225
JFELION DR SS	10 $\frac{1}{8}$	79.3	0.795	45,000	50,000	55,000	5,000	37,500

Connection	Size (inch)	Weight (lb/ft)	Pipe Body Wall (inch)	100, 105 ksi Grade Torque (ft-lb)				
				Final Torque			Shoulder Torque	
				Min	Opt	Max	Min	Max
JFELION CBR	9 $\frac{5}{8}$	53.5	0.545	26,300	29,220	32,140	2,922	21,915
JFELION DR ASM	10 $\frac{3}{4}$	85.3	0.797	51,210	56,900	62,590	5,690	42,675
JFELION DR SS	10 $\frac{1}{8}$	79.3	0.795	45,000	50,000	55,000	5,000	37,500

Connection	Size (inch)	Weight (lb/ft)	Pipe Body Wall (inch)	125 ksi Grade Torque (ft-lb)				
				Final Torque			Shoulder Torque	
				Min	Opt	Max	Min	Max
JFELION CBR	9 $\frac{5}{8}$	53.5	0.545	-	-	-	-	-
JFELION DR ASM	10 $\frac{3}{4}$	85.3	0.797	57,280	63,640	70,000	6,360	47,730
JFELION DR SS	10 $\frac{1}{8}$	79.3	0.795	45,000	50,000	55,000	5,000	37,500

13.8 End Finishing Requirements

OD (inch)	Classi- fication	Weight (lb/ft)		End Finish				
		Lower	Upper	High Chrome Steel Pin	9 to 13% Chrome Box	15% Chrome and above Box	Carbon Steel Pin	Carbon Steel Box
2 7⁄8	SD26	6.40	6.40	Bead Blast Mill & Field End	Clear- Plate™ (If Clear- Plate is not available, please contact JFETC)	Copper- Plate Or Clear-Plate	Bead Blast Mill & Field End	Manganese Phosphate Or Copper- Plate Or Clear-Plate
	SD30	7.80	9.35					
3 1⁄2	SD29	9.20	10.20					
	SD35	12.70	14.80					
4	SD35	11.60	16.10					
	SD29	11.60	12.60					
4 1⁄2	SD32	13.50	15.20					
	SD35	17.00	18.90					
	SD51	21.50	23.70					
5	SD30	15.00	15.00					
	SD36	18.00	21.40					
	SD38	23.20	24.10					
5 1⁄2	SD41	15.50	17.00					
	SD46	20.00	23.00					
	SD49	26.00	26.80					
	SD51	28.40	29.70					
6	SD45	22.80	22.80					
	SD50	32.00	32.00					
6.068	SD61	32.60	32.60					
	SD41	20.00	20.00					
6 5⁄8	SD49	24.00	32.00					
	SD54	40.20	40.20					
7	SD49	23.00	29.00					
	SD52	32.00	35.00					
	SD54	38.00	42.70					
7 7⁄8	SD47	26.40	29.70					
	SD52	33.70	39.00					
	SD57	42.80	42.80					
8 5⁄8	SD50	36.00	44.00					
	SD57	49.00	52.00					
	SD62	54.00	57.40					
9 5⁄8	SD51	40.00	43.50					
	SD57	47.00	59.40					
9 7⁄8	SD68	62.80	68.90					
10 3⁄4	SD56	45.50	51.00					
	SD65	55.50	73.20					
10 7⁄8	SD65	72.00	72.00					
11 3⁄4	SD62	60.00	71.00					
11 7⁄8	SD62	62.00	71.80					
	SD63	68.00	77.00					
13 3⁄8	SD65	80.70	86.00					
	SD68	92.00	92.00					
13 5⁄8	SD65	88.20	88.20					
14	SD66	93.00	93.00					
	SD68	100.00	115.0					
9 5⁄8	CBR	53.50	53.5					
10 1⁄8	DR SS	-	-					
10 3⁄4	DR ASM	-	-					
6 5⁄8	DRPB	-	-					
7 5⁄8	DRPB							

13.8.1 Clear Run End Finishing Requirements

OD (inch)	High Chrome¹ Steel Pin End Finish	High Chrome¹ Steel Box End Finish	Carbon Steel Pin End Finish	Carbon Steel Box End Finish
2 7⁄8" to 3 1⁄2"	Bead blast mill and field end	Clear-Plate	Bead blast mill and field end	Manganese phosphate
4 1⁄2" (up to 18.9#) to 5"	None			
4 1⁄2" (21.5 & 23.7#) to 5 1⁄2"	None		None	Clear-Plate
7" (29 & 32#)	Not applicable	Not applicable	Bead blast mill and field end	

Note¹ - Definition of high chrome steel: Containing ≥ 9%Cr

13.9 Molybdenum Disulphide Application

This table should be referenced when copper-plate has been applied to the JFELION box connection to confirm if Molybdenum Disulphide (MoS2) shall be applied to the pin & box seal and shoulder area prior to dope application.

OD (inch)	SD No.	Weight (lb/ft)		Apply MoS2	
		Lower	Upper	9-13%Cr	≥15%Cr
5	SD30	15	15	Not Applicable	Apply to pin and box seal and shoulder area
	SD36	18	21.4		
	SD38	23.2	24.1		
5 ½	SD41	15.5	17		
	SD46	20	23		
	SD49	26	26.8		
6	SD51	28.4	29.7		
	SD45	22.8	22.8		
6.068	SD50	32	32		
	SD61	32.6	32.6		
6 ⅝	SD41	20	20	Apply to pin and box seal and shoulder area	
	SD49	24	32		
	SD54	40.2	40.2		
7	SD49	23	29		
	SD52	32	35		
	SD54	38	42.7		
7 ⅝	SD47	26.4	29.7		
	SD52	33.7	39		
	SD57	42.8	42.8		
8 ⅝	SD50	36	44		
	SD57	49	52		
	SD62	54	57.4		
9 ⅝	SD51	40	43.5		
	SD57	47	59.4		
9 ⅞	SD68	62.8	68.9		
10 ¾	SD56	51	51		
	SD65	55.5	73.2		
10 ⅞	SD65	72	72		
11 ¾	SD62	60	71		
11 ⅞	SD62	62	71.8		
13 ⅜	SD63	68	77		
	SD65	80.7	86		
	SD68	92	92		
13 ⅝	SD65	88.2	88.2		
14	SD66	93	93		
	SD68	100	115		
9 ⅝	CBR	53.5	53.5		

13.10 Hydrostatic Test Fixtures

The JFELION hydrostatic test plug and cap design prevents metal to metal seal contact with accessory components due to the inclusion of an O-ring. The test cap and plug are also low torque designs. This section provides details for O-ring dimensions, assembly and inspection of the fixture.

The following points shall be noted when manufacturing JFELION Test Caps and Plugs:

- The following information shall be low stress stamped on all test fixtures. Size, Weight, SD number or special design designation and Maximum Working Pressure, the maximum pressure shall not exceed 10,000psi.

Example: 7" 29# JFELION SD49 P110 MWP: 10,000psi

Note: If the test cap or plug requires increased working pressure above 10,000psi, contact your local JFE-TC office.

- Test caps and plugs shall be manufactured from low alloy steel with a minimum yield strength of 110ksi and maximum yield strength of 140ksi.
- Higher rated Autoclave connections can be used instead of ½" NPT. But the maximum working pressure will remain limited to 10,000psi unless otherwise specified by the controlling center.

13.10.10-Ring Details

The following grade and dimensions of O-Ring material shall be used.

Designation	O-ring Size		O-ring Material
	Nominal	Actual	
Tubing	0.0625"	0.070" +/-0.003" (1.78mm)	NBR or Viton (90 Durometer)
Casing	0.125"	0.139" +/-0.004" (3.53mm)	

Note:

- Reference Parker O-Ring handbook guide for design, table 4-2.
- It is recommended that the O-Rings are moulded or spliced and vulcanized.
- It is recommended to discard the O-ring after single use.

13.10.2 O-ring Groove Diameters

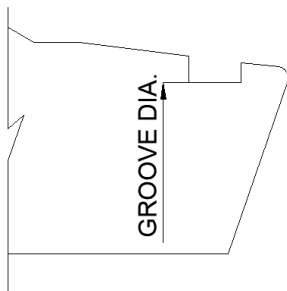


Figure 13.10.2.1 –
Test plug groove detail

13.10.3 Tubing test plug groove diameter

Size	Classification	Weight (lb/ft)		Groove Diameter
		Min	Max	
2 7/8"	SD26	6.4#	6.4#	2.6087
	SD30	7.8#	9.35#	2.5796
3 1/2"	SD29	9.2#	10.2#	3.2111
	SD35	12.7#	14.8#	3.1766
4"	SD35	11.6#	16.1#	3.6736
4 1/2"	SD29	11.6#	12.6#	4.2071
	SD32	13.5#	15.2#	4.1896
	SD35	17.0#	18.9#	4.1671
5"	SD30	15.0#	15.0#	4.6980
	SD36	18.0#	21.4#	4.6621
	SD38	23.2#	24.1#	4.6466

13.10.4 Casing test plug groove diameter

Size	Classification	Weight (lb/ft)		Groove Diameter
		Min	Max	
4 1/2"	SD51	21.5	23.7	3.9795
5 1/2"	SD41	15.5#	17.0#	5.0327
	SD46	20.0#	23.0#	5.0037
	SD49	26.0#	26.8#	4.9839
	SD51	28.4#	29.7#	4.9711
6"	SD45	22.8#	22.8#	5.5109
	SD50	32.0#	32.0#	5.4808
6.068"	SD61	32.6#	32.6#	5.4793
6 5/8"	SD41	20.0#	20.0#	6.1625
	SD49	24.0#	32.0#	6.1049
	SD54	40.2#	40.2#	6.0807
7"	SD49	23.0#	29.0#	6.4859
	SD52	32.0#	35.0#	6.4627
	SD54	38.0#	42.7#	6.4474
7 5/8"	SD47	26.4#	29.7#	7.1155
	SD52	33.7#	39.0#	7.0832
	SD57	42.8#	42.8#	7.0510
8 5/8"	SD50	36.0#	44.0#	8.0971
	SD57	49.0#	52.0#	8.0546
	SD62	54.0#	57.4#	8.0255
9 5/8"	SD51	40.0#	43.5#	9.0862
	SD57	47.0#	59.4#	9.0505
9 7/8"	SD68	62.8#	68.9#	9.2362
10 3/4"	SD56	51.0#	51.0#	10.1849
	SD65	55.5#	73.2#	10.1308
10 7/8"	SD65	72.0#	72.0#	10.2558

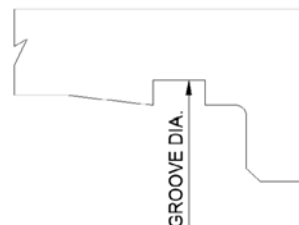


Figure 13.10.4.1 –
Test cap groove detail

13.10.5 Tubing test cap groove diameter

Size	Classification	Weight (lb/ft)		Groove Diameter
		Min	Max	
2 7/8"	SD26	6.4#	6.4#	2.8346
	SD30	7.8#	9.35#	2.8056
3 1/2"	SD29	9.2#	10.2#	3.4371
	SD35	12.7#	14.8#	3.4016
4"	SD35	11.6#	16.1#	3.9016
4 1/2"	SD29	11.6#	12.6#	4.4371
	SD32	13.5#	15.2#	4.4196
	SD35	17.0#	18.9#	4.3971
5"	SD30	15.0#	15.0#	4.9300
	SD36	18.0#	21.4#	4.8941
	SD38	23.2#	24.1#	4.8786

13.10.6 Casing test cap groove diameter

Size	Classification	Weight (lb/ft)		Groove Diameter
		Min	Max	
4 1/2"	SD51	21.5	23.7	4.4409
5 1/2"	SD41	15.5#	17.0#	5.5021
	SD46	20.0#	23.0#	5.4731
	SD49	26.0#	26.8#	5.4538
	SD51	28.4#	29.7#	5.4376
6"	SD45	22.8#	22.8#	5.9783
	SD50	32.0#	32.0#	5.9467
6.068"	SD61	32.6#	32.6#	5.9467
6 5/8"	SD41	20.0#	20.0#	6.6329
	SD49	24.0#	32.0#	6.5813
	SD54	40.2#	40.2#	6.5491
7"	SD49	23.0#	29.0#	6.9583
	SD52	32.0#	35.0#	6.9351
	SD54	38.0#	42.7#	6.9198
7 5/8"	SD47	26.4#	29.7#	7.5904
	SD52	33.7#	39.0#	7.5581
	SD57	42.8#	42.8#	7.5259
8 5/8"	SD50	36.0#	44.0#	8.5710
	SD57	49.0#	52.0#	8.5285
	SD62	54.0#	57.4#	8.4994
9 5/8"	SD51	40.0#	43.5#	9.5646
	SD57	47.0#	59.4#	9.5259
9 7/8"	SD68	62.8#	68.9#	9.7136
10 3/4"	SD56	51.0#	51.0#	10.6638
	SD65	55.5#	73.2#	10.6057
10 7/8"	SD65	72.0#	72.0#	10.7307

13.10.7 Installation of O-ring

Prior to installation of the O-ring, use a non-metallic brush with a liquid solvent to remove any storage compound.

The connection and body of the fixtures should be visually inspected for signs of any impact damage, corrosion etc.

- 1 Place the respective O-rings into the cap and plug grooves using suitable O-ring grease such as Parker O-Lube, see figures below.

Figure 13.10.7.1 – O-ring fitted (Plug)



Figure 13.10.7.2 – O-ring fitted (Cap)



- 2 API Modified or suitable thread compound shall be applied to all other areas except for the O-ring area, however it should be applied to the corresponding surface where the O-ring will contact once assembled, see figures below.

Figure 13.10.7.3 – Thread Compound (Plug)



Figure 13.10.7.4 – O-ring fitted (Cap)



13.10.8 Storage and Maintenance

After use, the fixtures should be thoroughly cleaned, dried and a suitable storage compound such as Kendex applied prior to installation of thread protectors. It is recommended that the fixtures be stored indoors and are not subjected to outdoor weather conditions.

It is recommended to perform NDE on the entire body of the fixture annually to check for any surface breaking and or sub-surface defects such as cracks.

13.10.9 Disclaimer

The users of these test caps and plugs are liable for the maintenance, use and safe operation. In no event shall JFE be liable for any damages, costs and expenses incurred in connection with the use of these test fixtures.

13.11 Special clearance OD dimensions

JFELION Special Clearance Coupling OD's					
Size (inch)	Weight (lb/ft)	Wall Thickness (inch)	SC80 (inch)	SC90 (inch)	Tolerance (inch)
2 7⁄8	6.40	0.217	3.203	3.242	+ 0.020 / - 0
	7.80	0.276	3.255	3.303	
	8.60	0.308	3.295	3.347	
	9.35	0.340	3.333	3.389	
3 1⁄2	9.20	0.254	3.867	3.913	
	10.20	0.289	3.914	3.966	
	12.70	0.375	3.993	4.057	
	14.30	0.430	4.058	4.129	
	14.80	0.449	4.080	4.153	
4 1⁄2	12.60	0.271	4.900	4.952	
	13.50	0.290	4.912	4.967	
	15.20	0.337	4.977	5.039	
	17.00	0.380	5.016	5.084	
	17.70	0.402	5.044	5.116	
	18.90	0.430	5.080	5.155	
	21.50	0.500	5.151	5.236	
5	23.70	0.560	5.221	5.313	
	15.00	0.296	5.434	5.490	
	18.00	0.362	5.496	5.563	
	21.40	0.437	5.596	5.674	
	23.20	0.478	5.636	5.719	
5 1⁄2	24.10	0.500	5.663	5.749	
	15.50	0.275	5.916	5.970	
	17.00	0.304	5.959	6.017	
	20.00	0.361	6.015	6.082	
	23.00	0.415	6.089	6.165	
	26.00	0.476	6.154	6.239	
	26.80	0.500	6.185	6.273	
	28.40	0.530	6.210	6.302	
6	29.70	0.562	6.250	6.346	
	22.80	0.375	6.544	6.614	
6.068	32.00	0.519	6.712	6.805	
6 5⁄8	32.60	0.553	6.770	6.868	
	20.00	0.288	7.072	7.128	
	24.00	0.352	7.122	7.190	
	28.00	0.417	7.215	7.294	
	32.00	0.475	7.296	7.383	
7	40.20	0.625	7.467	7.576	
	23.00	0.317	7.465	7.527	
	26.00	0.362	7.532	7.601	
	29.00	0.408	7.598	7.676	
	32.00	0.453	7.642	7.727	
	35.00	0.498	7.705	7.797	
	38.00	0.540	7.749	7.847	
	42.70	0.625	7.861	7.971	

JFELION Special Clearance Coupling OD's					
Size (inch)	Weight (lb/ft)	Wall Thickness (inch)	SC80 (inch)	SC90 (inch)	Tolerance (inch)
7 5⁄8	26.40	0.328	8.115	8.180	+ 0.020 / - 0
	29.70	0.375	8.186	8.258	
	33.70	0.430	8.238	8.320	
	35.80	0.465	8.288	8.376	
	39.00	0.500	8.338	8.431	
8 5⁄8	42.80	0.562	8.396	8.499	
	36.00	0.400	9.212	9.290	
	40.00	0.450	9.286	9.372	
	44.00	0.500	9.358	9.453	
	49.00	0.557	9.403	9.507	
	52.00	0.595	9.456	9.566	
9 5⁄8	54.00	0.625	9.472	9.588	
	57.40	0.656	9.515	9.635	
	40.00	0.395	10.203	10.281	
	43.50	0.435	10.263	10.349	
	47.00	0.472	10.285	10.377	
	53.50	0.545	10.392	10.496	
9 7⁄8	58.40	0.595	10.464	10.576	
	59.40	0.609	10.483	10.598	
	62.80	0.625	10.735	10.852	
	65.30	0.650	10.770	10.892	
	66.40	0.661	10.785	10.909	
	66.90	0.668	10.795	10.920	
10 3⁄4	67.50	0.678	10.809	10.935	
	68.00	0.694	10.831	10.960	
	68.90	0.700	10.839	10.969	
	51.00	0.450	11.424	11.513	
	55.50	0.495	11.441	11.538	
	60.70	0.545	11.516	11.621	
10 7⁄8	65.70	0.595	11.589	11.703	
	73.20	0.672	11.699	11.826	
	72.00	0.656	11.803	11.927	
11 3⁄4	60.00	0.489	12.455	12.522	
	65.00	0.534	12.523	12.628	
	71.00	0.582	12.595	12.708	
11 7⁄8	62.00	0.500	12.597	12.696	
	71.80	0.582	12.720	12.833	
13 3⁄8	68.00	0.480	14.067	14.163	
	72.00	0.514	14.120	14.222	
	77.00	0.550	14.175	14.284	
	80.70	0.580	14.206	14.321	
	85.00	0.608	14.248	14.368	
	86.00	0.625	14.274	14.396	
13 5⁄8	92.00	0.672	14.330	14.460	
	88.20	0.625	14.525	14.648	
14	93.00	0.650	14.937	15.065	
	100.00	0.700	14.998	15.134	
	114.00	0.800	15.144	15.296	
	115.00	0.812	15.161	15.315	

14.1 Pipe Calculations

14.1.1 Plain end weight

$$W_{pe} = K_m \times K_{wpe} \times (D - t)t$$

Where:

D = specified pipe outside diameter in millimetres or inches

K_m = mass correction factor, 1.000 for carbon steel; 0.989 for martensitic chromium steel

K_{wpe} = mass per unit length conversion factor, 0.0246615 for SI units; 10.69 for USC units

t = specified pipe wall thickness

W_{pe} = calculated plain end mass per unit length, in kilograms per metre or pounds per foot

14.1.2 Maximum internal yield pressure (MIYP) 'burst pressure'

$$MIYP = \frac{2 \times SMYS}{D} \times t \times f$$

Where:

MIYP = Maximum internal yield pressure (psi)

SMYS = Specified minimum yield stress (psi)

t = specified pipe wall thickness (inch)

D = specified pipe outside diameter (inch)

f = factor for minimum allowed wall thickness (usually 0.875 = 87.5%)

14.1.3 Pipe body yield strength (PBYS)

$$PBYS = SMYS \times Area_{pipe}$$

Where:

SMYS = Specified minimum yield stress (psi)

Areapipe = cross section area of pipe body (inch), calculated as $\pi/4 (OD^2 - ID^2)$

OD = specified pipe outside diameter (inch)

ID = specified pipe inside diameter (inch)

14.1.4 Coupling bearing face load for JFE connections

$$Load\ bearing\ face = 0.9 \times SMYS \times (\pi/4 (CBD^2 - CED^2))$$

Where:

SMYS = Specified minimum yield stress (psi)

CBD = Coupling diameter at base of bevel (20deg) or chamfer (45deg) (inch)

ID = Coupling entry diameter (inch)

14.2 Field Calculations

14.2.1 Buoyed weight

$$\frac{W_{bouyed}}{W_{air}} = \frac{\rho_{mud}}{65.5}$$

Where:

W_{air} = string weight in air, calculated as length $\times$ linear mass (inch)

ρ_{mud} = density of mud (ppg)

14.2.2 Downhole hydrostatic pressure

$$P = 0.052 \times TVD \times W_{mud}$$

Where:

P = downhole hydrostatic pressure, external or internal (psi)

TVD = downhole vertical depth of interest (ft)

W_{mud} = density of mud (ppg)

14.2.3 Change in axial stress due to bending

$$\Delta\sigma_{bending} = 218.166 \times \alpha \times OD$$

Where:

$\Delta\sigma_{bending}$ = change in axial stress (psi), (+) on outside and (–) on inside

α = bending dogleg in degrees per 100ft

OD = outside diameter of pipe body (inch)

14.2.4 Additional load due to bending

$$\Delta\sigma_{bending} = \sigma_{bending} \times Area_{pipe}$$

Where:

$\Delta F_{bending}$ = Actual load applied due to bending (lbs)

$\sigma_{bending}$ = bending stress

$Area_{pipe}$ = cross section area of pipe body (inch), calculated as $\pi/4 (OD^2 - ID^2)$

OD = specified pipe outside diameter (inch)

ID = specified pipe inside diameter (inch)

14.2.5 Change in axial load due to internal pressure ('ballooning')

$$\Delta F_{axial} = P_{internal} \times \pi/4 \times d^2$$

Where:

ΔF_{axial} = Change in axial load applied due to internal pressure (lbs)

$P_{internal}$ = Internal pressure applied (psi)

d = specified pipe inside diameter (inch)

14.2.6 Pipe stretch

$$\Delta L = \frac{P_{load} \times L_{free}}{E \times Area_{pipe}}$$

Where:
ΔL = Change in string length (ft)
P_{load} = Force applied (lbs) i.e. string weight
L_{free} = Free length of pipe (ft)
E = Young’s modulus (30x10⁶)
Area_{pipe} = cross section area of pipe body (inch), calculated as π/4 (OD² – ID²)
OD = specified pipe outside diameter (inch)
ID = specified pipe inside diameter (inch)

14.2.7 Pipe displacement

$$Displacement_{pipe} = Area_{pipe} \times 0.001237$$

Where:
Displacement_{pipe} = displacement of pipe (bbl/ft)
Area_{pipe} = cross section area of pipe body (inch), calculated as π/4 (OD² – ID²)
OD = specified pipe outside diameter (inch)
ID = specified pipe inside diameter (inch)

14.2.8 Pipe capacity

$$Capacity_{pipe} = (ID_{pipe})^2 \times 0.000971439$$

Where:
Capacity_{pipe} = capacity of pipe string (bbl/ft)
ID_{pipe} = ID = specified pipe inside diameter (inch)

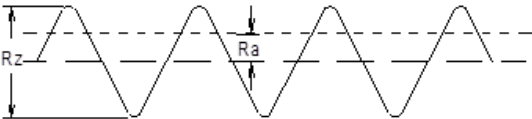
14.2.9 Pipe capacity

$$Capacity_{pipe} = (Area_{pipeID})^2 \times 0.001237$$

Where:
Capacity_{pipe} = capacity of pipe string (bbl/ft)
Area_{pipeID} = calculated as π × (ID_{pipe} / 2)² (inch)

14.3 Other

14.3.1 Calculating surface finish values



Where:
R_z = maximum peak to valley variation on surface substrate, i.e. max value – min value
R_a = arithmetic average deviation from nominal surface, i.e. **Ra = R_z / 7.2**

14.4 Common conversion factors

Mass	1	lb _m	=	0.4536	kg
		kg	=	2.2046	lb
		Short ton	=	2000	lbs
		Short ton	=	0.9072	MT
		MT	=	1.1023	Short Ton
		lb/ft	=	1.4882	kg/m
Area	1	kg/m	=	0.672	lb/ft
		in ²	=	645.16	mm ²
		mm ²	=	0.00155	in ²
		ft ²	=	0.0929	m ²
Volume	1	m ²	=	10.7639	ft ²
		gallon	=	231	in ³
		gallon	=	0.0038	m ³
		gallon	=	3.7854	litre
		bbl	=	42	gal
		bbl	=	158.987	litre
		litre	=	61.0237	in ³
		litre	=	0.2642	gal
		m ³	=	6.2899	bbl
		m ³	=	264.172	gal
		in ³	=	0.0164	litre
		ft ³	=	1728	in ³
		ft ³	=	28.317	litre
		ft ³	=	0.0283	m ³
		ft ³	=	7.4805	gal
Length	1	in	=	25.4	mm
		mm	=	0.03937	in
		cm	=	0.3937	in
		ft	=	0.3048	m
		m	=	39.37	in
		m	=	3.2808	ft
Force	1	lb _f	=	4.4482	N
		N	=	0.2248	lb _f
		ton _f	=	8.896	kN
		kN	=	224.81	lb _f
Torque	1	ft-lb	=	1.3558	N-m
		ft-lb	=	0.13826	Kg-m
Pressure	1	atm	=	14.696	psi
		atm	=	101.325	kPa
		MPa	=	10	bar
		MPa	=	145.038	psi
		kPa	=	0.145	psi
		psi	=	6.8948	kPa
		psi	=	0.0069	MPa
		psi	=	0.0689	bar
		bar	=	14.5038	psi
		bar	=	0.1	MPa
		bar	=	100	kPa
Density	1	lb/gal	=	0.1198	kg/l
		lb/gal	=	119.826	kg/m ³
		lb/ft ³	=	16.018	kg/m ³
		kg/l	=	8.3454	lb/gal
		kg/m ³	=	0.0083	lb/gal
		kg/m ³	=	0.0624	lb/ft ³